

DARL McCULLOUGH
DAVID J. NOVLAN



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			WSMR 1974
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			WSMR 1970

April Temperatures

Volumary 3-W Complement Winds ---

June 5-M Commune Vinds -----

PART 2 VEWELCAL PROPERS

INTRODUCTION

Rocketsonde atmospheric data for the 25-65 km levels at White Sands Missile Range (WSMR), New Mexico over the period 1961-1975 is the basis of two sections - Data and Modeling. The purpose of this report is to provide the upper portion of a complete atmospheric structure and a data base for projects such as balloon systems, rocket systems, lifting re-entry vehicles, missile detection system and high energy lasers.

Section I is data by month for the years 1961-1975. Standard Deviations are included by month for the years 1969-1975 extracted from "High Altitude Meteorological Data" reports (Reference 12). The extreme Standard Deviations for 25 and 26 km December 1969-1975 N-S, E-W winds do not follow the monthly or height trend 20 km to 30 km, so these four values are suspect.

Modeling in Section II is presented with emphasis on E-W wind component and the changeover cycle. A few cases of actual changeovers are presented for comparison with the model.

Rockets launched at Small Missile Range (SMR), provide a period of record of 1961-1975 with accuracies of instrumentation and the resulting data as stated in reference 9. SMR is located in the southern portion of WSMR (Figure 1).

SMR physical data = a. latitude 32° 28' N

b. longitude 106° 25' W

c. elevation 1,219 m MSL*

*MSL is measured above sea level.

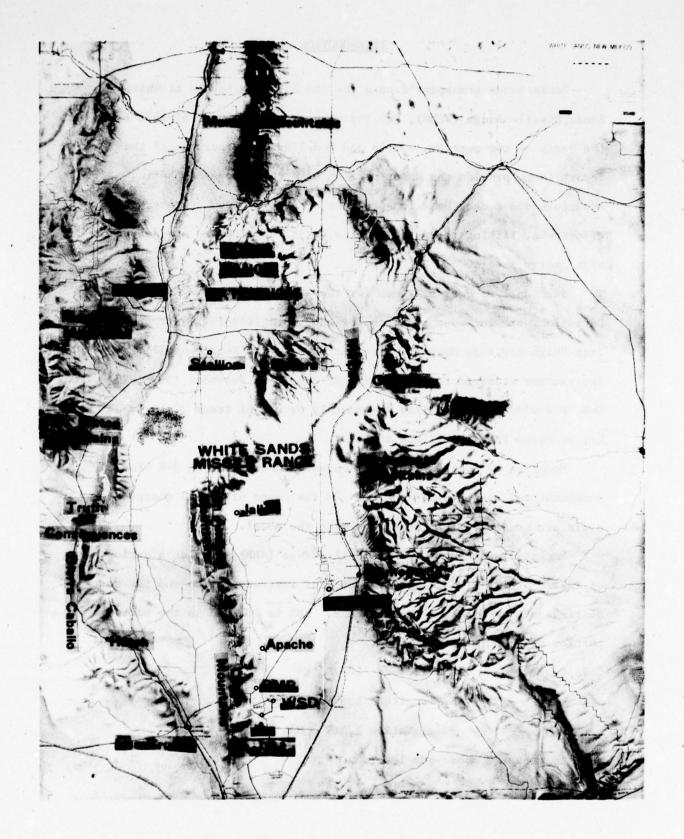


FIGURE 1. MAP OF METEOROLOGICAL SITES AT WSMR

EXPLANATION OF TERMS

1. WIND COMPONENTS

Average zonal and meridional components for the month are calculated.

A wind from the south or west is designated by a positive value, while a wind from the north or east is designated by a negative value. A zonal wind is from the east or west, a meridional from the north or south.

2. WIND GUSTS

Wind gusts are characterized by sudden, intermittent increases in speed, with at least five meters per second variation between peaks and lulls. The average time interval between peaks and fulls usually should not exceed 20 seconds.

3. TEMPERATURE

Average temperatures for the month for the given altitude are in degrees Celsius.

4. PRESSURE

Average pressures for the month for the given altitudes are in millibars.

5. DENSITY

Average densities for the month for the given altitude are in grams per cubic meter.

SECTION I PART 1

Rocketsonde data by month at WSMR is averaged 1961-1975 with standard deviations given for 1969-1975 portion in Tables 1-12.

Note that the numerical values for the standard deviations for temperatures, E-W, N-S Wind Components are larger in the winter (January and December) compared to summer (July and August). This may be attributed to the wintertime long and short term reversals which can cause considerable fluctuations in the temperature and wind fields. Long term reversals may be related to sudden warming episodes more prominent in the higher latitudes.

	TARIF

| DENS. | STD | DEV. | 1.085 | .914 | .731 | . 594 | .523 | 864. | 757

 | 370

 | 0/6 | .348 | .324 | .316 | .296 | .263 | .227 | .194

 | .167 | .152 | 137

 | 751 | 111 | .110

 | .097 | .088 | 080

 | 990 | 090
 | .054 | .050 | .048 | .043 | .039
 | .035 | .032
 | .029 | .026 | .024 | .022
 | .019 | 910. | .014 | .012 | 600. |
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PRESS	STD	DEV.

 | 107.

 | 2007 | .242 | .218 | .200 | .182 | .165 | .146 | .138

 | .126 | 115 | 101

 | 100 | 260. | 980.

 | .079 | .071 | 790

 | 056 | 050
 | 970. | .041 | .039 | .034 | .030
 | .027 | .025
 | .022 | .020 | .018 | .016
 | .015 | .013 | .012 | .011 | 800. |
| TEMP STD | DEV. | | 3.6 | 3.9 | 0.4 | 4.2 | 4.7 | 5.2 | 2 2

 | 0.0

 | 2.9 | 6.1 | 6.7 | 8.9 | 8.2 | 8.9 | 9.6 | 9.7

 | 9.3 | 6.0 |

 | 0.0 | 0., | 8.2

 | 7.9 | 7.1 | 4.4

 | 0 | 9
 | 5.6 | 5.4 | 5.9 | 8.9 | 8.9
 | 9.9 | 8.9
 | 7.1 | 7.9 | 8.2 | 9.2
 | 6.6 | 9.5 | 7.6 | 8.6 | 10.3 |
| STD | 4 | HIE | 10.1 | 11.6 | 13.1 | 14.7 | 15.5 | 16.6 | 10,

 | 7.01

 | 17.0 | 19.6 | 21.7 | 22.8 | 22.3 | 23.1 | 23.2 | 23.7

 | 23.0 | 23.7 | 200

 | 67.0 | 24.0 | 25.3

 | 56.6 | 28.1 | 78.7

 | 29.0 | 30.6
 | 31.0 | 30.1 | 30.8 | 30.2 | 30.2
 | 29.3 | 29.4
 | 29.4 | 29.3 | 29.1 | 29.1
 | 29.1 | 30.9 | 29.4 | 28.5 | 36.7 |
| MIND | DEV. | 2-0 | 4.1 | 9.4 | 4.7 | 5.3 | 7.1 | 7.6 | 0

 | 0.0

 | 0. | 8.2 | 8.7 | 8.6 | 0.6 | 9.6 | 10.3 | 10.0

 | 11.5 | 11.8 | 12.0

 | 13.4 | 12.0 | 12.0

 | 16.1 | 18.0 | 19.3

 | 19.0 | 20.9
 | 19.9 | 19.3 | 19.1 | 18.1 | 18.2
 | 19.6 | 19.9
 | 22.2 | 22.3 | 19.6 | 20.0
 | 19.6 | 19.5 | 19.4 | 21.9 | 20.0 |
| TOTAL | OBSNS | | 96 | 113 | 120 | 122 | 125 | 128 | 101

 | 121

 | 171 | 128 | 124 | 127 | 128 | 126 | 127 | 125

 | 123 | 123 | 123

 | 121 | 171 | 123

 | 122 | 121 | 121

 | 119 | 113
 | 115 | 116 | 114 | 111 | 109
 | 106 | 102
 | 66 | 96 | 89 | 80
 | 67 | 61 | 53 | 47 | 36 |
| MEAN | DENSITY
G/CII M | 2 00 15 | 39.723 | 33.821 | 28.821 | 24.563 | 20.962 | 17.922 | 15 919

 | 13 003

 | 13.093 | 11.200 | 9.573 | 8.202 | 7.031 | 6.036 | 5.186 | 4.464

 | 3.843 | 3 322 | 220.0

 | 2 507 | 7.00.7 | 2.192

 | 1.916 | 1.685 | 1.485

 | 1.311 | 1.161
 | 1.028 | .914 | .812 | .717 | .634
 | .560 | .495
 | .437 | .386 | .339 | .298
 | .260 | .228 | .201 | .176 | .153 |
| TOTAL | OBSNS | | | | 199 | | | |

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 | | | |
 | | 61 | 53 | 47 | 36 |
| MEAN | PRESS | | 24.850 | 21.311 | 18.283 | 15.687 | 13.482 | 11.608 | 200

 | 9.995

 | 8.620 | 7.447 | 6.435 | 5.578 | 4.846 | 4.213 | 3.672 | 3.212

 | 2.804 | 2 456 | 2.430

 | 2.130 | 1.890 | 1.674

 | 1.476 | 1.303 | 1.150

 | 1.014 | .897
 | .792 | 869. | .539 | .540 | .475
 | .417 | .366
 | .323 | .283 | .249 | .218
 | .190 | .166 | .145 | .126 | .109 |
| | OBSNS | | 66 | 119 | 129 | 130 | 134 | 137 | 100

 | 136

 | 130 | 137 | 133 | 136 | 138 | 136 | 136 | 135

 | 133 | 134 | 101

 | 134 | 131 | 133

 | 132 | 131 | 130

 | 128 | 122
 | 124 | 125 | 122 | 119 | 117
 | 111 | 107
 | 103 | 97 | 89 | 80
 | 29 | 61 | 53 | 47 | 36 |
| MEAN | DEG C | | -55.3 | -54.0 | -52.2 | -50.8 | -49.2 | -47.5 |

 | -45.8

 | -43.7 | -41.3 | -38.9 | -36.2 | -33.2 | -30.1 | -26.7 | -22.5

 | -19.0 | 15.5 | 15.5

 | -12.7 | 7.6- | -6.5

 | -4.5 | -3.4 | -3.1

 | -3.7 | -4.1
 | -5.4 | -7.3 | -9.0 | -10.8 | -11.9
 | -13.8 | -15.0
 | -16.4 | -17.1 | -17.8 | -18.5
 | -18.9 | -19.3 | -20.6 | -23.2 | -23.9 |
| TOTAL | OBSNS | | 224 | 259 | 264 | 269 | 272 | 278 | 000

 | 283

 | 284 | 284 | 282 | 283 | 285 | 286 | 285 | 284

 | 281 | 281 | 107

 | 617 | 9/7 | 276

 | 274 | 267 | 260

 | 260 | 252
 | 247 | 252 | 546 | 245 | 240
 | 232 | 225
 | 219 | 210 | 197 | 189
 | 163 | 148 | 126 | 115 | 103 |
| MIND | N-E | | 4 | 3 | 4 | 2 | - | - α |

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 | = | 13 | 15 | 17 | 18 | 10 | 20 | 202

 | 22 | 7,0 | 47

 | 07 | 97 | 31

 | 34 | . 88 | 40

 | 42 | 43
 | 77 | 94 | 94 | 41 | 84
 | 64 | 21
 | 24 | 25 | 28 | 61
 | 65 | 65 | 89 | 72 | 74 |
| MEAN | S-N | | 0 | 0 | 0 | - | ١- | | 1

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 | 74 | £. | 77

 | 45 | 46 | 47

 | 84 | 67
 | 20 | 51 | 52 | 2 | 4 :
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 | 61 | 62 | 63 | 99 | 65 |
| | MEAN WIND TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL WIND STD TEMP STD PRESS | N WIND TOTAL MEAN TOTAL MEAN TOTAL WIND STD TEMP STD PRESS PS MPS OBSNS TEMP OBSNS PRESS OBSNS DENSITY OBSNS DEV. BEV. STD W-E DEG C MRS CACH M C M C M C M C M C M C M C M C M C M | MEAN WIND TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL WIND STD TEMP STD PRESS COMPS MPS OBSNS TEMP OBSNS PRESS OBSNS DENSITY OBSNS DEV. DEV. STD S-N W-E DEC C MBS MBS G/CU M S-N W-E DEV. | MEAN WIND TOTAL MEAN TOTAL MEAN TOTAL WIND STD TEMP STD PRESS COMPS MPS OBSNS TEMP OBSNS PRESS OBSNS DENSITY OBSNS DEV. DEV. STD S-N W-E DEG C MBS G/CU M S-N W-E DEV. 0 4 224 -55.3 99 24.850 94 39.723 94 4.1 10.1 3.6 .602 1 | MEAN WIND TOTAL MEAN TOTAL MEAN TOTAL WIND STD TEMP STD PRESS COMPS MPS OBSNS TEMP OBSNS PRESS OBSNS DEN. DEV. STD STD PRESS OBSNS DEV. DEV. STD STD DEG C MBS G/CU M S-N W-E DEV. DEV. DEV. DEV. OBSNS DEV. DEV. DEV. OBSNS DEV. DEV. OBSNS DEV. DEV. OBSNS DEV. DEV. DEV. OBSNS DEV. DEV. OBSNS DEV. DEV. DEV. OBSNS DEV. DEV. DEV. DEV. OBSNS DEV. DEV. DEV. DEV. OBSNS DEV. DEV. DEV. DEV. DEV. DEV. DEV. DEV. | MATAN WIND TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL WIND STD TEMP STD PRESS S-N W-E DEG C MBS G/CU S-N W-E DEV. DEV. DEV. 0 4 224 -55.3 99 24.850 94 39.723 94 4.1 10.1 3.6 .602 1 0 3 259 -54.0 119 21.311 113 33.821 113 4.6 11.6 3.9 .509 0 4 264 -52.2 129 18.283 121 28.821 120 4.7 13.1 4.0 .442 | MEAN WIND TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MIND STD TEMP STD PRESS COMPS MPS OBSNS DENSITY OBSNS DEV. STD STD S-N W-E DEC MBS G/CU M S-N W-E DEV. DEV. 0 4 224 -55.3 99 24.850 94 39.723 94 4.1 10.1 3.6 .602 1 0 3 259 -54.0 119 21.311 113 33.821 113 4.6 11.6 3.9 .509 0 4 264 -52.2 129 18.283 121 28.821 120 4.7 13.1 4.0 .442 1 5 269 -50.8 130 15.687 122 24.563 122 5.3 14.7 4.2 2.7 2375 | MATAN WIND TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL WIND STD TEMP STD PRESS COMPS MPS OBSNS DENSITY OBSNS DEV. STD STD STD STD STD DEV. DEV. | MATAN WIND TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MIND STD TEMP STD PRESS S-N W-E DEG C MBS G/CU M S-N W-E DEV. STD 0 4 224 -55.3 99 24.850 94 39.723 94 4.1 10.1 3.6 .602 1 0 3 259 -54.0 119 21.311 113 33.821 113 4.6 11.6 3.9 .509 0 4 264 -52.2 129 18.283 121 28.821 120 4.7 13.1 4.0 .442 1 5 269 -50.8 130 15.687 122 24.563 122 5.3 14.7 4.2 .375 1 5 269 -50.8 134 13.482 128 <t< th=""><th>MATHON TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL WIND TOTAL WIND STD TEMP STD PRESS S-N W-E DEG C DES C C C C DEV. STD PRESS S-N W-E DEG C DEG C DEV. STD DEV. STD 0 4 224 -55.3 99 24.850 94 39.723 94 4.1 10.1 3.6 .602 1 0 4 264 -55.2 129 18.283 121 28.821 120 4.7 13.1 4.0 .442 1 5 269 -50.8 130 15.687 122 24.563 122 5.3 14.7 4.2 .375 1 7 272 -49.2 13.482 128 27.5 15.5 27.5<!--</th--><th>MAIND TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MIND TOTAL WIND TOTAL WIND STD TEMP STD PRESS S-N W-E DEG C DEG C DEV. STD PRESS S-N W-E DEG C DEG C DEV. STD 0 4 224 -55.3 99 24.850 94 39.723 94 4.1 10.1 3.6 .602 1 0 4 264 -52.2 129 18.283 121 28.821 120 4.7 13.1 4.0 .442 1 5 269 -50.8 130 15.687 122 24.563 122 5.3 14.7 4.2 .375 1 7 272 -49.2 13.482 125 20.962 125 7.1 15.2 5.2 5.2 5.2</th><th>MATHOL TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MIND TOTAL WIND STD TEMP STD PRESS S-N W-E DEG C MBS G/CU A S-N W-E DEV. STD O 4 224 -55.3 99 24.850 94 39.723 94 4.1 10.1 3.6 .602 1 0 4 264 -52.2 129 18.283 121 28.821 120 4.6 11.6 3.9 .509 0 4 264 -52.2 129 18.283 121 28.821 120 4.7 13.1 4.0 .442 1 5 269 -50.8 130 15.687 122 24.563 122 5.3 14.7 4.2 .375 1 7 272 -49.2 13.482 125</th><th>MATOL MEAN TOTAL MIND TOTAL MIND STD TEMP STD S-N W-E DEG C MBS G/CU A S-N W-E DEV. STD 0 4 224 -55.3 99 24.850 94 39.723 94 4.1 10.1 3.6 .602 10 0 4 264 -52.2 129 18.283 121 28.821 120 4.7 13.1 4.0 .402 .602 10 1 5 269 -50.8 130 15.687 122 24.563 122 5.3 14.7 4.0 .442 1 7 272 -49.2 134 13.482 125 20.962 125 7.1 15.5 7.1 15.5 7.1</th><th>MATOL MEAN TOTAL MIND TOTAL MEC STD PRESS OBSNS DEV. STD DEV. STD DEV. STD 0 4 224 -55.3 99 24.850 94 39.723 94 4.1 10.1 3.9 509 509 60.0</th><th>MATOL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MIND TOTAL WIND TOTAL MIND TOTAL MEC STD PRESS OBSNS DEV. STD DEV. STD 0 4 224 -55.3
 99 24.850 94 39.723 94 4.1 10.1 3.9 509 509 60.0</th><th>COMPS MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MIND TOTAL MIND STD TEMP STD S-N W-E DEG C MBS C/CU M S-N W-E DEV. STD 0 4 224 -55.3 99 24.850 94 39.723 94 4.1 10.1 3.6 509 0 4 224 -55.2 129 18.283 121 28.821 120 4.7 13.1 4.0 14.2 0 4 264 -52.2 129 18.283 122 24.563 122 5.3 14.7 4.2 .402 1 5 269 -50.8 130 15.687 122 24.563 122 5.3 14.7 4.2 .339 2 20 -60.8 134 13.482 125 20.962 125</th><th>COMPS MFS OBSNS TOTAL MEAN TOTAL MIND TOTAL MEAN TOTAL MIND TOTAL MIND STD TEMP STD PRESS S-N W-E DEG MBS C/CU M S-N W-E DEV. STD 0 4 224 -55.3 99 24.850 94 39.723 94 4.1 10.1 3.6 509 0 4 264 -52.2 129 18.283 121 28.821 120 4.7 13.1 4.0 .602 1 0 4 264 -50.8 130 15.687 122 24.563 122 24.51 4.7 13.1 4.0 .442 1 7 272 -49.2 134 13.482 125 24.563 125 125 <</th><th>COMPS WEAN WIND TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL WIND STD TEMP STD PRESS COMPS WA-E DEG C MBS G/CU M S-N W-E DEV. STD S-N W-E DEG PRESS OBSNS PRESS OBSNS DENSITY OBSNS DEV. S-N W-E DEV. DEV. DEV. DEV. STD 0 4 224 -55.3 199 24.850 94 39.723 94 4.1 10.1 3.6 509 0 4 264 -52.2 129 18.283 121 28.821 120 4.6 11.6 3.9 .509 1 5 269 -50.8 130 15.687 122 24.563 122 4.6 11.6 3.9 .509 2 6 6 13.482 122<!--</th--><th>WIND TOTAL MEAN TOTAL MIND STD TEMP STD PRESS S-N W-E DEG PRESS OBSNS PRESS OBSNS DEV BDV DEV S-N W-E DEG PRESS OBSNS DEVS BDV DEV 0 4 224 -55.3 199 24.850 94 39.723 94 4.1 10.1 3.6 20.2 0 4 264 -52.2 129 11.3 33.821 11.0 3.6 6.0 4.1 10.1 3.6 9.0 1 5 269 -50.8 130 11.608 122 24.563 122 24.563 122 24.563 122 24.563 122 4.2 4.2 4.2 4</th><th>OMEAN WIND TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MIND TOTAL WIND TOTAL MIND TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN DEG COMENS PRESS OBSNS DEG DEG</th><th>OMPS WEAN TOTAL MEAN PRESS OBSNS PRESS OBSNS PRESS OBSNS PRESS OBSNS DEG <t< th=""><th>MEAN WIND TOTAL MEAN TOTAL WIND TOTAL WIND STD PRESS S-N W-E DBC DBC C MBS G/CU M S-N M-E DBV. STD 0 4 224 -55.3 199 24.850 94 39.723 94 4.1 10.1 3.9 .602 190 0 4 264 -52.2 129 18.283 121 28.3 4.1 10.1 3.9 .602 1 1 5 269 -50.8 130 15.687 122 24.563 122 4.1 10.1 3.9 .402 14.4 1 2 264 -50.2 13 13.482 122 24.563 122 24.563 122 24.563 122 4.1 10.1 3.9</th><th>MEAN WIND TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL WIND STD PRESS COMPS NFS 085NS PRESS 085NS DEV. DEV.</th><th>OMES WIND TOTAL MEAN TOTAL MEAN TOTAL MIND TOTAL MIND TOTAL MEAN TOTAL MEAN TOTAL MIND TOTAL MIND TOTAL MIND TOTAL MIND TOTAL MES Same Color PRESS OBSINS DENSITY OBSINS DENSITY OBSINS DENSITY DEN PRESS OBSINS DENSITY OBSINS DEN DEN PRESS OBSINS DENSITY OBSINS DEN DEN<th>OFFICIAL MEAN TOTAL MEAN TOTA</th><th>OFFICIAL MEAN TOTAL MEAN TOTA</th><th>MEAN MIND TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MIND TOTAL WIND TOTAL WIND TOTAL WIND TOTAL WIND SEN S-N M-E OBSINS TEMP OBSINS PRESS OBSINS DEG PRESS PRESS<th>COLYPS OBSINS TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MEAN TOTAL MIND TOTAL WIND TOTAL WIND TOTAL PRESS OBSINS TEMP OBSINS DEV. DEV. DEV. STD DEV. DEV. STD DEV. DEV.</th><th>OFFICIAL MEAN TOTAL MEAN TOTA</th><th>OFFICIAL MEAN TOTAL MEAN TOTA</th><th>WEAN VIND TOTAL MEAN M</th><th>Order WIND TOTAL IRRAN TOTAL WEAN TOTAL TOTAL</th><th>Object WIND TOTAL IRRAN TOTAL MEAN MEAN MEAN TOTAL MEAN MEAN MEAN TOTAL MEAN MEAN</th><th>ORAFA WIND TOTAL MEAN MEAN<!--</th--><th>Order WEAR TOTAL NEAN TOTAL Sent G-10 G-10 Sent TOTAL NEAN NEAN</th><th>WEAR WIND TOTAL MEAN MEAN MEAN</th><th>WEAR WIND TOTAL MEAN PORTAL Sent PORTAL DEV. Sent COLOR A-1 10.1 3.6 20.0 10.0 A-1 10.1 3.6 3.0</th><th>ORACIT WEAR TOTAL NEAN NEAN</th><th>NEAN TOTAL NEAN NEAN</th><th>OWEST REAL TOTAL NEAN TOTAL VINE <t< th=""><th>OCKET PRANT PROTAL VICAL NEAR TOTAL NEAR</th><th>OWEST PRIAND TOTALL REAS TOTALL VINAD TOTALL REAS TOTALL NUMB TOTALL
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DENS. STD DEV.	1.046	.803	200.	214	474	435	80%	201	.359	.314	.266	.256	.235	.210	.179	.147	.127	.109	860.	.085	.084	920.	.071	.064	.057	.050	.045	.041	.036	.034	.031	.028	.027	.022	.020	.017	.014	.014	110.	.012	.010
PRESS STD DEV.	.553	994.	014.	231	1000	267	107.	C+7.	.223	.199	.182	.162	.146	.130	.118	.110	101.	.093	980.	070.	.071	790.	.058	.052	.047	.043	.039	.035	.031	.030	.026	.024	.022	.020	.016	.014	.013	.012	.01	.011	600.
- 1975 STD																																									
TEMP DEV.	3.6	e .	v. 4	1.0	**	4 n		1.0	6.1	6.0	5.9	6.8	7.3	7.8	8.3	8.5	8.5	7.7	7.0	6.4	7.9	6.2	5.6	5.8	5.8	5.8	5.9	5.7	6.2	6.3	6.7	7.1	7.1	7.3	7.4	7.6	7.7	7.8	8.0	8.0	6.8
STD W-E	9.6	10.1	9.11	12.3	17.4	17.3	5.71	18.1	19.5	20.8	21.9	23.4	24.0	24.7	25.2	25.9	30.0	28.7	29.3	28.1	27.7	27.4	26.4	25.6	25.3	23.9	24.7	26.0	25.7	27.3	28.0	27.9	27.2	23.9	23.2	22.6	24.6	26.3	27.4	28.1	27.3
WIND DEV.	3.5	4.3	4.5	5.1	2.0	0	6.1	3												12.8			14.6	15.7	15.9	15.8	15.1	15.9	15.7	16.1	17.0	17.1	17.5	19.2	18.5	18.0	17.9	19.3	20.5	19.7	20.5
TOTAL	112	129	140	145	150	150	151	151	151	150	150	151	151	151	151	150	150	149	150	149	150	148	144	144	142	142	142	137	138	137	133	129	126	121	115	111	76	8	75	65	20
MEAN DENSITY G/CU M	30 701	33.861	28.852	24.550	20.922	17.789	15,158	12.931	11.048	9.460	8.113	6.997	6.037	5.216	4.518	3.907	3 30%	2 055	203	2 261	1070	1 738	1 533	1 354	1 105	1.057	936	.829	. 733	. 648	. 575	502	877	395	876	302	07.0	230	010	185	.163
TOTAL	112	129	140	145	150	150	151	151	151	150	150	151	151	151	151	150	150	149	150	149	150	148	144	144	142	142	142	137	138	137	133	129	126	121	115	111	76	85	75	65	20
FEBRUARY MEAN PRESS MBS	24.850	21.315	18.271	15.684	13.475	11.595	10.013	8.666	7.494	905.9	5.656	4.930	4.299	3.756	3.287	2.877	2.524	2.219	1.952	1.721	1.515	1.333	1.175	1.038	916	808	.713	.631	.556	064.	.432	.380	.335	.294	.258	.226	.198	.174	.153	.134	.117
1975 FF TOTAL OBSNS	123	139	150	155	160	160	191	162	162	191	191	162	162	162	162	191	161	160	160	159	160	157	153	152	148	147	146	141	142	140	135	130	126	121	115	111	96	82	75	65	20
1961 - MEAN TEMP DEG C	-55.0	-54.0	-52.4	-50.3	-48.4	-45.8	-45.9	-39.4	-36.5	-33.3	-30.0	-27.5	-24.9	-21.9	-19.2	-16.3	-13.7	-11.2	-9.2	-7.0	-5.6	-5.2	-5.1.	-5.1	-5.6	7.9-	-7.4	-7.6	-8.6	-9.7	-11.0	-12.2	-13.0	-14.1	-15.2	-16.7	-18.6	-19.8	-20.5	-21.6	-23.6
TOTAL	242	270	275	282	283	288	297	298	296	295	295	596	596	293	293	290	285	284	283	283	282	281	280	278	275	273	272	797	256	253	546	244	237	229	214	205	188	173	153	130	113
WIND MPS W-E	7	7	4	· ·		æ ;	9	7:	2 :	7	13	77	77	54	25	25	56	28	30	32	35	36	38	04	42	43	77	45	47	64	64	27	52	24	28	09	9	67	67	99	99
MEAN COMPS S-N	7	7	7.	7.	7.	7 .		٥.	٠.	٠,	7	7.	7 .	7'	7-	0	0	-	-	e	4	5	•	1	7	۲,	œ (x 0 (10 1	- 0	ות	- 1	- '	6	0	10	6	9	4	7	-5
ROCKET- SONDE	25	520	17	200		3.5	100	33	3 2	200	25	9 2	200	8 8	36	040	41	42	43	44	45	94	47	48	69	20	21	52	53	54	55	26	57	58	59	09	61	62	63	. 49	65

STO.	1.328	.785	78. CES	.457	.390	.349	S.	. 289	222	139	.174	.157	.138	621.	77.	2	98	.078	88		.055	85.5	3	8.	8	.028	8	ਰ ਹ	.018	910.	3 5	100	3 8	8	8	graph of the
1975 PRESS STD STD DEV.	.648 .49 5	.415	319	.291	. 263	.239	.219	.201	169	152	.139	.128	.116	.105	400	. 970	896.	.061	.055	050.	24.	039	. E.O.	8.	.028	.024	.021	.018	.016	*10.	*0.	70.	§ §	8	8.	
1969 - 1 TEMP SI DEV.	3.7	4.2	 	4.6	¥.4	5.4	5.6	6.2	7.6	, m.	5.4	6.0	6.2	6.2	ب د ه	הים	5.2	5.4	5.2	4.9	5,3	5.1) ·	8.	4.7	5.2	5.7	S.5	6.0			0 4 0 4	* *	o r) ,
SID F	6.6	•			2.	14.5	16.9	20.6	16.7	17.7	18.0	19.2	19,7	20.0	25.2	22.7	21.5	20.5	20.2	20.3	18.2	18.2	9 0	19.4	19.3	19.2	19.8	20.3	22.4	23.7	25.2	25.7	23.5	¥ 7 7 6 6	23.2	
WIND DEV. S-N	3.5	4.0	0.4	4.3	•	•	•	7.5			•	8.4	9.0	4.6	ور د در د	70.7	11.2	11.9	12.8	13.1	12.8	12.9	7.71	12.8	13.0	13.3	13.7	13.2	14.9	16.6	17.3	0.0	16.1	10.0 10.0	15.6)
TOTAL	97	123	132	131	133	131	132	132	130	131	131	131				130						126														
NEAN DENSITY G/CU M	39.683 33.844	28.842	20.943	17.866	15.269	13.078	11.203	9.615	7.138	6.161	5,332	4.615	4.002	3.477	3.027	2.638	2.023	1.775	1,562	1.377	1.214	1.070	. 944. 020	739	.654	.578	.511	.452	.399	.353	.311	.273	.241	217.	163	
TOTAL	97 112	123	132	131	133	131	132	132	130	131	131	131	132	132	131	131	132	131	132	128	127	126	57.	126	123	119	118	113	108	107	93	*	22	£ (2 6	3
MARCH NEAN PRESS MBS	25.014 21.490	18.655	13.665	11.778	10.182	8.810	7.635	6.630	5 021	4.379	3.824	3.344	2.929	2.569	2.254	1.983	1.538	1,356	1.195	1.058	.933	.822	97/	266	499	.439	.387	.340	. 299	. 262	.230	.201	.177	.155	.135	011.
- 1975 : TOTAL OBSNS	101 116	127	139	138	141	139	140	140	141 138	138	138	138	139	139	138	138	138	137	137	133	132	131	130	131	128	124	122	117	112	110	105	88	92	73	200	3
1961 - NEAN IEMP DEG C	. . .	9.67	0.04-	-43.5	-40.9	-38.4	-35.7	-32.8	130.4	-25.5	-23.1	-20.5	-18.0	-15.5	-13.4	-11.2	1.61	-7.0	-5.5	-5.5	-5.3	-5.2	-5.1	-6.3	-7.2	-8.4	-9.4	-10.5	-11.8	-13.4	-15.0	-16.4	-18.1	-19.6	-20.9	6.17-
TOTAL	211 246	254	797 767	273	273	272	273	272	077	271	270	267	264	263	262	767	757		256	253	250	243	238	232	229	221	216	212	200	187	174	153	138	119	106 95	2
WIND MPS W-E	m 4	ıo ı	~ σ	20	12	13	16	19	217	24	25	26	79	56	27	78	£ 6		32	32	33	34	<u>ئ</u> ج	3,5	36	37	38	33	41	41	9	41	42	66	£ 6	9
XEAN COMPS S-N	0 1	~ (7 F	d pod	7	2	2	7		4 0	0	0	0	0	7	m <	† 4	· W		. 9	7	7		۰ ۰	· 0	. α	7	9	7	7	7	•	S.	. 7	4 -	4
ROCKET- SONDE	25 26	27	28	7 Q	31	32	33	፠	35	37	; æ	39	60	41	42	£3 :	44	£ 4	47	48	69	ያ :	7 2	7 E	7 7	55	26	57	58	89	8	19	62	63	3 3	C D

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DENS.	DEV.	105	885	732	.597	501	417	374	335	297	269	237	220	506	186	165	148	138	123	104	.089	920	990	190	.053	940	.043	038	035	030	.027	026	.022	020	.018	015	013	012	011	600	
		i				•	•	•			•							•														•									
PRESS STD	DEV.	.660	. 538	.459	.385	.338	.304	.277	.250	.229	.207	.187	.168	.149	.133	.117	.105	.093	.084	.080	990.	.059	.053	.048	.043	.037	.034	.032	.027	.024	.022	.019	.018	.017	.015	.014	.012	.010	010	.010	
1969 - 1975 TEMP STD DEV.		2.8	3.0	3.1	3.6	3.8	4.1	4.3	4.0	4.3	4.5	4.2	4.1	4.0	4.0	4.2	4.4	6.4	5.1	6.4	8.4	4.5	4.4	4.1	3.8	3.4	3.4	3.7	3.7	4.0	4.0	4.2	3.9	4.4	4.6	6.4	5.4	5.9	6.1	6.3	
STD	W-E	4.3	4.4	4.6	5.3	5.5	6.5	7.2	7.7	8.5	9.1	4.6	10.2	11.3	12.2	13.4	14.6	14.4	15.5	14.6	15.6	16.3	16.6	17.4	17.8	17.9	17.7	18.2	18.6	18.3	17,4	19.7	19.6	19.6	20.7	19.8	20.2	21.4	20.7	21.7	
WIND DEV.	S-N	5.9	3.2	5.6	3.1	3.4	4.1	4.6	5.2	5.2	0.9	6.1	9.6	6.1	6.9	7.4	8.3	0.6	8.9	6.7	8.5	8.2	8.3	9.5	10.8	6.7	8.7	6.7	8.2	8.9	6.3	12.2	13.1	12.0	11.7	12.6	12.8	12.8	11.6	14.7	
TOTAL		85	66	106	115	119	120	120	120	119	117	120	120	120	120	120	120	119	118	119	117	119	118																		
MEAN	G/cu M	40.243	34.229	29.230	24.962	21.324	18.233	15.619	13.368	11.447	9.852	7.875	7.321	6.321	5.461	4.731	4.099	3.561	3.102	2.704	2.365	2.076	1.822	1.604	1.417	1.252	1.107	.981	898.	.769	.681	.604	.535	.475	.422	.372	.329	.291	.256	.226	
TOTAL	7.5	85	66	106	115	119	120	120	120	119	117	120	120	120	120	120	120	119	118	119	117	119	118	117	116	115	113	111	108	108	101	105	102	96	91	91	82	80	89	59	
APRIL MEAN PRESS	MBS	25.593	21.964	18.900	16.256	14.012	12.101	10.462	9.061	7.858	6.839	5.941	5.177	4.517	3.947	3.455	3.029	2.659	2.340	2.062	1.816	1.602	1.414	1.248	1.104	926.	862	.762	.673	.594	.524	.462	.407	.359	.317	.279	.245	.215	.188	.165	
1975 A TOTAL OBSNS																		128	127	128	126	128	127	126	125	123	121	119	116	116	114	111	108	102	96	95	88	84	72	63	
1961 - MEAN TEMP	DEG C	-51.5	-49.5	6.74-	-46.2	-44.2	-41.8	-39.7	-36.8	-33.9	-31.6	-29.4	-26.6	-23.9	-20.9	-18.2	-15.0	-12.1	-9.5	-7.0	6.4-	-3.6	-2.3	-1.5	-1.2	-1.1	-1.4	-1.9	-2.5	-3.3	4.4-	-5.8	-7.5	-8.8	-10.1	-11.8	-13.2	-14.6	-15.8	-16.7	
TOTAL		210	239	258	264	797	270	273	273	272	276	281	279	281	280	277	277	275	273	270	272	270	797	263	260	259	256	253	546	241	237	232	226	215	202	192	177	164	155	139	
WIND	W-E	0	-	6	4	9	1	6	9	12	14	16	11	17	17	16	15	14	13	13	14	14	13	13	13	17	12	=	1	10	6	0	1	9	9	2	2	4	*	3	
MEAN	N-S	1	1	1	1	-	1	1	-	2	-	1	-1	0	-		0	2	3	4		2	2	. 9	2	4		2	2	2	4	3	2	9	1	7	7	9	1	9	•
ROCKET- SONDE		25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	20	51	52	53	54	55	26	57	58	59	09	61	62	63	

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	DENS.	STD DEV.	1.321	1.004	.831	.703	.612	.519	944.	.380	.315	.285	.254	.224	.206	.178	.157	.142	.131	.113	660.	.083	.074	.070	090.	.050	.043	.039	.034	.032	.029	.026	20.	.019	.020	910.	.017	.015	.014	.011	.010	.010	.010
		DEV.	.816	.637	.543	.467	.412	.360	.313	.275	.243	.216	.194	.172	.153	.134	.119	.108	960.	.084	.074	.067	.061	.054	.048	.043	.038	.037	.033	.029	.027	.023	170.	.018	.017	910.	.015	.013	.012	.011	.011	.010	.010
1969 - 1975	TEMP STD	DEV.	2.0	2.0	2.0	2.3	2.8	2.8	3.0	2.9	5.6	5.6	3.0	3.5	5.9	3.4	3.9	3.5	3.6	3.6	3.7	3.2	3.2	3.2	3.5	3.6	3.9	4.3	4.1	3.9	4.0	4.2	7.4	7.7	4.3	4.4	8.4	5.2	5.2	5.4	6.1	9.9	8.9
	STD	H-E	3.4	5.2	5.0	5.0	5.7	6.1	8.9	7.9	9.1	11.0	11.1	8.8	8.7	7.8	7.8	9.1	6.6	10.4	10.8	13.4	15.0	16.3	11.2	11.4	11.2	6.7	10.5	10.2	10.5	12.7	11.0	11.7	11.	10.9	13.7	14.6	14.7	13.6	13.9	14.6	16.5
		S-N	2.9	3.0	2.9	2.9	3.1	3.6	3.7	3.7	3.9	5.5	10.8	10.1	6.2	4.2	9.4	8.4	5.3	9.4	6.3	7.1	8.1	10.2	7.2	6.7	7.9	8.0	6.3	5.9	7.0	4.6	2.0	8.2	4.8	0.6	10.4	2.6	8.4	10.1	10.9	11.8	11.9
	TOTAL	OBSNS	06	108	113	119	117	121	123	124	125	125	124	123	124	123	123	124	123	123	123	123	123	123	123	122	122	122	121	118	116	115	113	114	113	113	110	66	76	68	80	63	20
	MEAN	G/CU M	898.07	34.817	29.735	25.419	21.765	18.625	15.950	13.683	11.744	10.112	8.836	7.534	6.493	2.607	4.854	4.206	3.649	3.175	2.770	2.425	2.126	1.874	1.654	1.463	1.295	1.146	1.015	006.	. 798	.708	979	.557	.493	.437	.386	.341	.300	.265	.235	.207	.181
	TOTAL	CNCGO	06	108	113	119	117	121	123	124	125	125	124	123	124	123	123	124	123	123	123	123	123	123	123	122	122	122	121	118	116	115	113	114	113	113	110	66	76	88	80	63	20
MAY	MEAN	MBS	26.157	22.462	19.330	16.659	14.373	12.409	10.731	9.304	8.072	7.014	6.102	5.320	4.643	4.063	3.558	3.120	2.740	2.410	2.124	1.873	1.653	1.463	1.294	1.146	1.014	868.	.793	.700	.618	.545	184.	.424	.374	.329	.289	.253	.221	.194	.170	.148	.128
1975	TOTAL	chicao	96	113	111	127	125	129	132	133	134	134	134	133	135	134	134	135	134	134	134	134	133	133	132	131	131	131	130	126	125	123	121	121	120	120	116	105	100	94	82	99	20
1961 -	MEAN	DEG C	-50.3	-48.6	-46.7	-45.1	-43.2	-41.2	-38.9	-36.4	-33.8	-31.6	-29.0	-27.3	-24.0	-20.8	-17.7	-14.7	-11.6	-8.5	-6.0	-4.0	-2.1	-1.0	0	5.3	٠:	3.8	7	-1.8	-3.1	9.4-	-6.3	-7.9	-9.5	-11.2	-13.2	-14.9	-17.5	-19.4	-21.7	-24.6	-28.6
	TOTAL	CNCCO	230	259	277	283	285	291	290	594	300	299	302	302	303	536	536	306	305	305	303	302	303	300	297	295	291	588	286	281	280	277	717	260	253	247	236	227	210	192	173	142	116
	WIND	W-E	4-	-3	-3	-5	7	7	7	0	0	0	0	7	7	-3	-5	9	8-	6-	-12	-13	-14	-12	-15	-16	-18	-19	-20	-20	-22	-22	-73	-25	-26	-28	-28	-30	-32	-33	-32	-32	-33
	MEAN	S-N	-	1	-	-	0	0	1	7	7	1	-	1	0	0	0	0	-	1	7	3	3	4	4	. 4	4	4	S	5	2	٠.	4 .	4	4	4	3	3	4	9	9	9	4
	ROCKET-		25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	946	47	48	49	20	51	52	23	7.	25	8	27	28	59	09	61	62	63	99	65

DENS. STD DEV.	1.814	1.467	1.197	096.	.799	.707	.622	1.639	.445	.379	.337	.289	.243	.211	.179	.159	.132	.117	.102	960.	.082	.073	.068	.062	.053	.046	.038	.034	.031	.027	.025	.024	.023	.020	.016	.016	.016	.015	.014	.012	.009	
PRESS STD DEV.	1.098	.894	.740	.611	.518	.448	.389	.332	.288	.253	.219	.191	.166	.146	.129	.114	660.	060.	.080	.075	.063	.056	.051	.046	.040	.037	.032	.030	.027	.024	.022	.019	.019	.017	.016	.014	.014	.013	.012	110.	.008	
1969 - 1975 TEMP STD DEV.	1.9	2.3	2.2	2.4	2.4	2.5	2.8	2.8	2.9	3.1	3.0	3.3	3.2	3.3	3.3	3.4	3.5	4.0	4.0	3.9	3.7	3.5	4.0	4.7	8.4	4.7	4.7	4.5	4.7	4.7	6.4	2.0	5.2	5.4	5.8	9.9	7.0	7.1	7.8	9.6	4.6	
STD	3.5	8.8	8.3	8.2	8.4	8.8	9.5	4.6	9.5	0.6	0.6	9.5	8.6	8.9	9.5	9.4	6.6	10.7	9.5	9.1	4.6	10.7	10.8	8.6	8.6	10.1	9.6	9.5	11.2	11.8	17.0	12.3	11.2	13.0	14.6	17.5	18.4	18.7	17.9	17.5	18.5	
WIND DEV.	2.4	2.7	5.6	5.6	3.0	3.3	3.9	4.0	4.1	4.5	3.8	3.6	0.4	3.5	4.1	6.4	8.4	5.4	9.6	5.5	5.9	8.9	7.5	9.9	7.5	7.1	7.4	8.3	7.4	8.3	8.8	6.6	10.3	6.7	10.6	11.8	12.3	14.3	14.5	15.4	19.5	
TOTAL	92	111	119	127	129	130	130	132	133	133	132	132	132	131	131	130	132	132	132	132	132	131	129	131	130	130	129	128	125											73	28	
MEAN DENSITY G/CU M	41.699	35.563	30.377	25.952	22.260	19.066	16.348	13.936	12.073	10.392	8.956	7.723	6.672	5.778	5.007	4.345	3.774	3.281	2.859	2.502	2.194	1.929	1.700	1.504	1.333	1.180	1.044	.926	.821	.728	949.	.573	. 508	.450	.399	.354	.313	.278	.246	.216	.189	
TOTAL	92	111	119	127	129	130	130	132	133	133	132	132	132	131	131	129	132	132	132	132	132	131	129	131	130	130	129	128	125	125	124	123	118	119	118	109	100	91	82	73	28	
JUNE MEAN PRESS MBS	26.808	23.056	19.855	17.114	14.776	12.764	11.049	9.579	8.311	7.225	6.287	5.482	4.788	4.191	3.670	3.221	2.830	2.489	2.251	1.933	1.705	1.506	1.333	1.180	1.044	.923	.816	.721	.636	.560	767.	.436	.384	.338	.298	.262	.230	.202	.177	.154	.133	
TOTAL OBSNS	95	114	123	134	137	139	139	141	142	142	141	141	141	139	139	138	140	140	140	140	139	138	136	138	136	136	135	134	131	131	130	129	124	125	123	114	104	95	84	74	28	
1961 - MEAN TEMP DEG C	0.64-	-47.1	-45.3	-43.2	-41.8	-39.9	-37.6	-35.3	-33.2	-30.7	-28.3	-25.6	-22.9	-20.1	-17.5	-14.4	-11.6	-8.5	-20.0	-3.8	-2.3	6	.1	2		4	6	-1.9	-3.2	6.4-	-6.7	-8.4	-10.2	-11.7	-13.8	-15.9	-18.5	-20.5	-22.9	-24.8	-28.6	
TOTAL	226	255	270	272	273	281	282	286	288	767	767	292	294	262	292	291	289	288	290	588	289	287	286	288	287	285	283	282	279	274	268	262	255	243	234	219	196	178	156	131	114	* 100000
WIND MPS W-E	-10	7	-15	-15	-13	-13	-14	-14	-15	-16	-17	-17	-19	-21	-22	-24	-26	-29	-31	-32	-33	-35	-36	-37	-38	-39	-40	-42	-43	-45	94-	-48	64-	-51	-53	-55	-57	-57	-58	-58	09-	
MEAN COMPS S-N		-	0	1	-	1	7	1	1	-	1	-		1	1		1	-	-	7	2	3	4	4	9	2	2	2	2	2	4	3	3	3	3	2	4	4	3	9	4	
ROCKET- SONDE	25	56	27	28	29	30	31	32	33	34	35	36	37	38	39	9	41	42	43	44	45	949	47	84	64	20	51	52	53	54	55	26	57	58	59	09	19	62	63	94	65	

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90 26.998 89 42.208 82 3.5 4.9 2.7 .567 1.057 116 23.363 115 36.083 108 3.3 4.1 2.7 1.377 1.893 115 21.378 1189 115 22.546 115 36.083 108 3.3 4.1 2.7 1.377 1.893 115 21.378 1189 117.330 122 22.546 115 3.6 4.5 3.1 3.5 6.96 1.528 1125 11.938 122 12.536 115 3.6 4.5 3.1 3.5 6.96 1.528 1125 11.938 122 12.536 115 4.6 5.1 4.8 2.8 1.060 1.528 1125 11.939 124 16.617 117 4.0 4.8 3.5 6.96 9.44 1127 11.939 124 12.254 115 4.6 5.1 4.0 4.8 3.5 6.94 1.337 11.6 5.37 11.6 5.37 11.6 5.37 11.6 5.37 11.6 5.37 11.6 5.3 1.0 5.8	
ABS G/CU M S=N W=E DEV. 26.98 89 42.208 82 3.5 4.9 2.7 .567 23.363 115 36.083 108 3.3 4.1 2.7 .157 21.091 117 30.797 110 4.3 4.8 2.8 1.060 17.330 121 26.337 114 3.8 4.5 3.6 4.5 3.6 12.928 122 12.436 115 3.9 4.3 3.5 .696 11.933 124 16.617 117 4.6 5.1 4.7 .106 11.933 124 16.617 117 4.6 5.1 4.7 .106 11.93 124 117 4.6 5.1 4.7 .104 12.93 124 117 4.8 5.7 4.7 .104 4.09 124 117 4.8 5.7 4.7 .104 4.10 125	TOTAL MEAN OBSNS TEMP
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119 1.709 116 7.3 7.9 4.0 .093 118 1.509 115 7.0 8.3 4.4 .084 116 1.334 114 7.2 9.5 4.7 .074 113 1.046 112 7.7 9.6 4.7 .061 113 1.046 112 7.7 11.7 4.8 .064 113 .927 112 7.7 11.7 4.8 .064 113 .927 112 7.7 11.1 5.9 .049 114 .728 110 9.9 11.1 5.7 .045 108 .572 107 10.9 11.6 5.7 .045 108 .572 107 10.0 13.1 5.9 .036 109 .349 95 13.1 18.8 6.9 .026 100 .349 95 16.6 24.3 7.6 .029 100 .349 95 16.6 24.3 7.6 .020 100 .349 95 16.6 24.3 7.6 .020 100 .349 95 16.6 24.3 7.6 .020 100 .349 95 16.6 24.3 7.6 .020 100 .349 95 16.6 24.3 7.6 .020 100 .349 95 16.6 24.3 7.6 .020 100 .349 95 16.6 24.3 7.6 .020 100 .349 95 16.6 24.3 7.6 .020 100 .349 95 16.6 24.3 7.6 .020 100 .349 95 16.6 24.3 7.6 .020 100 .349 95 16.6 24.3 7.6 .020 100 .349 95 16.6 24.3 7.6 .018 100 .349 95 16.6 24.3 7.6 .016 100 .349 95 16.6 24.3 7.6 .016	
118 1.509 115 7.0 8.3 4.4 .084 116 1.334 114 7.2 9.5 4.7 .074 113 1.046 112 7.7 9.6 4.7 .061 113 .927 112 7.7 11.7 4.8 .054 112 .821 111 8.8 10.9 5.3 .049 111 .728 110 9.9 11.1 5.7 .049 108 .645 107 10.0 11.6 5.7 .049 108 .572 107 10.0 11.6 5.7 .045 108 .572 107 10.0 11.6 5.7 .039 109 .572 107 10.2 12.3 16.0 6.2 .035 109 .349 99 13.1 18.8 6.9 .026 96 .349 95 16.0 6.4 .026 96 .349 95 16.0 6.2 .026 81	-3.5
110 11334 114 7.2 9.5 4.7 0.04 111 1181 114 7.8 10.2 4.6 0.06 112 11046 112 7.7 11.7 4.8 0.06 112 112 111 8.8 10.9 5.3 0.04 127 112 111 8.8 10.9 5.3 0.04 128 111 17.8 11.1 5.7 0.04 128 108 .645 107 10.0 11.6 5.7 0.04 129 108 .572 107 10.0 11.6 5.7 0.04 137 108 .572 107 10.2 13.1 5.9 0.03 138 108 .572 107 10.2 12.3 16.0 6.2 0.03 139 .448 102 12.3 16.0 6.3 .02 125 96 .349 95 16.0 6.3 .02 127 89 13.0 13.2 1	2.0
113 1.046 112 7.7 9.6 4.7 .061 113 1.046 112 7.7 9.6 4.7 .061 113 .927 112 7.7 11.7 4.8 .054 111 .728 110 9.9 11.1 5.7 .045 108 .572 107 10.0 11.6 5.7 .036 108 .507 107 10.8 17.5 6.2 .032 100 .396 99 13.1 18.8 6.9 .026 96 .349 95 16.6 24.3 7.6 .023 181 .270 81 16.9 27.7 7.5 .020 181 .270 81 16.9 27.7 7.5 .020 182 .210 59 24.8 31.8 7.8 .016	3.6
. 712 113 1.040 112 7.7 11.7 4.8 .054 .054 .057 112 113 .927 112 7.7 11.7 4.8 .054 .055 .055 .112 .728 110 9.9 11.1 5.7 .045 .045 .429 108 .545 107 10.0 11.6 5.7 .045 .378 108 .507 107 10.0 11.6 5.7 .039 .378 108 .507 107 10.2 12.3 16.0 6.3 .029 .255 96 .349 95 16.6 24.3 7.6 .025 .222 89 .306 88 17.3 24.5 7.7 .021 .189 81 .270 81 16.9 27.7 7.5 .020 .151 59 .210 59 24.8 31.8 7.8 .016 .151 59 .210 59 24.8 31.8 7.8 .016 .151 .185 43 23.0 34.7 7.6 .016	0.01
	263 -4.4 116
. 553 111 . 728 110 9.9 11.1 5.7 . 045	-7.2
.487 108 .645 107 10.0 11.6 5.7 .039 .429 108 .572 107 11.2 13.1 5.9 .036 .378 108 .507 107 10.8 17.5 6.2 .032 .333 103 .448 102 12.3 16.0 6.3 .029 .297 100 .396 99 13.1 18.8 6.9 .026 .255 96 .349 95 16.6 24.3 7.6 .023 .222 89 .306 88 17.3 24.5 7.7 .021 .189 81 .270 81 16.9 27.7 7.5 .020 .172 76 .238 76 21.9 32.0 7.8 .018 .151 59 .210 59 24.8 31.8 7.8 .016	-8.5
.429 108 .572 107 11.2 13.1 5.9 .036 .378 108 .507 107 10.8 17.5 6.2 .032 .297 100 .396 99 13.1 18.8 6.9 .029 .255 96 .349 95 16.6 24.3 7.6 .023 .222 89 .306 88 17.3 24.5 7.7 .021 .189 81 .270 81 16.9 27.7 7.5 .020 .172 76 .238 76 21.9 32.0 7.8 .016 .151 59 .24.8 31.8 7.8 .016 .131 43 .185 43 23.0 34.7 7.6 .016	-10.3
.378 108 .507 107 10.8 17.5 6.2 .032 .333 103 .448 102 12.3 16.0 6.3 .029 .297 100 .396 99 13.1 18.8 6.9 .026 .222 89 .306 88 17.3 24.5 7.7 .021 .189 81 .270 81 16.9 27.7 7.5 .020 .172 76 .238 76 21.9 32.0 7.8 .016 .151 59 .24.8 31.8 7.8 .016 .131 43 .185 43 23.0 34.7 7.6 .016	-12.0
103 .448 102 12.3 16.0 6.3 .029 100 .396 99 13.1 18.8 6.9 .026 96 .349 95 16.6 24.3 7.6 .023 89 .306 88 17.3 24.5 7.7 .021 81 .270 81 16.9 27.7 7.5 .020 76 .238 76 21.9 32.0 7.8 .018 59 .210 59 24.8 31.8 7.8 .016 43 .385 43 23.0 34.7 7.6 .016	-13.8
100 .396 99 13.1 18.8 6.9 .026 96 .349 95 16.6 24.3 7.6 .023 89 .306 88 17.3 24.5 7.7 .021 81 .270 81 16.9 27.7 7.5 .020 76 .238 76 21.9 32.0 7.8 .018 59 .210 59 24.8 31.8 7.8 .016 43 .385 43 23.0 34.7 7.6 .016	-15.5
96 .349 95 16.6 24.3 7.6 .023 89 .306 88 17.3 24.5 7.7 .021 81 .270 81 16.9 27.7 7.5 .020 76 .238 76 21.9 32.0 7.8 .018 59 .210 59 24.8 31.8 7.8 .016 43 .185 43 23.0 34.7 7.6 .016	-17.6
. 222 89 . 306 88 17.3 24.5 7.7 . 021 .189 81 . 270 81 16.9 27.7 7.5 . 020 .172 76 . 238 76 21.9 32.0 7.8 . 018 .151 59 . 210 59 24.8 31.8 7.8 . 016 .131 43 . 185 43 23.0 34.7 7.6 . 016	-19.2
81 .270 81 16.9 27.7 7.5 .020 76 .238 76 21.9 32.0 7.8 .018 59 .210 59 24.8 31.8 7.8 .016 43 .185 43 23.0 34.7 7.6 .016	-20.4
76 .238 76 21.9 32.0 7.8 .018 59 .210 59 24.8 31.8 7.8 .016 43 .185 43 23.0 34.7 7.6 .016	-21.5
59 .210 59 24.8 31.8 7.8 .016 43 .185 43 23.0 34.7 7.6 .016	
43 .185 43 23.0 34.7 7.6 .016	
	103 -25.4 4

	DENS	STD	DEV.	2.149	1.578	1.307	1.092	.956	.803	.679	.580	. 505	.442	.388	.341	.289	.248	.217	.195	.174	.157	.135	.118	.106	.094	.083	.074	990.	.056	.051	.044	.040	.037	.032	.028	.026	.024	.019	.015	.015	.013	.01	.010	.010
	PRESS	STD	DEV.	1.308	.988	.823	.706	.610	.524	.457	.398	.351	.310	.272	.240	. 209	.185	.163	.145	.130	.114	.103	060.	080	.071	.065	.057	.051	970.	.041	.036	.033	.029	.026	.023	.021	.020	.016	.015	.015	.012	.010	.010	.010
1969 - 1975		DEV.		3.1	2.7	5.6	2.5	2.7	2.8	3.2	3.3	3.8	3.9	3.8	3.7	3.5	3.4	4.0	4.0	4.4	5.4	5.1	4.5	4.4	4.7	5.0	8.4	4.5	4.5	6.4	4.7	4.3	5.2	5.1	9.6	5.9	4.9	6.7	7.3	7.8	7.9	8.6	9.8	8.9
	STD		W-E	3.0	3.1	3.5	3.8	3.4	3.6	4.0	6.4	5.6	5.3	5.2	5.4	6.2	7.2	7.6	11.2	8.4	4.6	9.5	6.6	10.4	10.3	10.6	11.0	11.7	12.8	13.1	15.1	16.7	16.9	17.6	21.3	20.4	21.0	21.4	22.2	24.0	26.2	25.0	23.5	28.0
	WIND	DEV.	N-S	2.5	5.9	2.5	5.6	3.4	3.4	3.4	3.3	4.1	3.7	4.3	4.3	3.8	9.4	2.0	4.9	6.4	5.5	5.7	7.3	7.1	7.5	4.8	9.1	9.3	10.0	10.9	11.1	11.7	11.3	12.5	8.6	12.5	14.5	14.3	13.9	13.9	14.8	17.0	18.8	20.4
	TOTAL	OBSNS		92	112	118	118	118	120	120	120	120	120	120	119	121	120	120	120	119	120	119	119	118	119	117	117	116	115	115	116	115	115	113	110	108	104	103	96	78	72	62	23	43
	MEAN	DENSITY	G/cu M	41.825	35.706	30.523	26.090	22.342	19.132	16.410	14.078	12.134	10.448	9.008	7.766	6.694	5.774	4.988	4.319	3.745	3.254	2.832	2.468	2.161	1.897	1.666	1.465	1.292	1.144	1.008	.891	.788	669.	.618	.549	.483	.427	.377	.334	.295	.259	.228	.200	.176
	TOTAL	OBSNS		107	126	132	132	132	134	134	134	134	134	134	133	135	133	133	133	130	131	130	129	127	127	124	123	120	117	117	118	116	115	113	110	108	104	103	96	78	72	62	53	43
AUGUST	MEAN	PRESS	MBS	26.833	23.078	19.844	17.094	14.740	12.678	11.013	9.537	8.262	7.167	6.230	5.425	4.719	4.114	3.592	3.142	2.756	2.413	2.126	1.869	1.647	1.450	1.278	1.126	1.020	.877	.773	.626	.602	.531	.467	.410	.361	.317	.278	.244	.214	.186	.162	.141	.124
	TOTAL	OBSNS		108	127	133	133	133	135	135	135	135	135	135	134	136	134	134	134	131	132	131	130	128	128	125	124	121	118	118	119	117	116	114	==	109	105	104	97	79	73	63	54	77
1961 -	MEAN	TEMP	DEG C	-50.1	-48.4	6.94-	-45.2	-43.6	-41.7	-39.7	-37.8	-36.1	-34.3	-32.3	-30.2	-27.6	-25.2	-22.3	-19.5	-16.8	-14.3	-11.5	-9.5	-7.5	9.9-	-5.7	5.1	-5.0	-5.4	-5.9	0.9-	-7.3	-8.6	6.6-	-11.3	-12.9	-14.5	-16.4	-18.2	-20.6	-23.3	-24.7	-26.0	-27.7
	TOTAL	OBSNS		263	280	289	292	292	295	297	298	596	293	293	293	767	291	284	283	281	278	274	274	271	569	569	569	263	262	256	254	546	546	241	237	230	217	208	189	159	145	125	111	88
	MIND	MPS	3-1	-16	-17	-17	-18	-19	-20	-20	-20	-21	-21	-21	-22	-23	-24	-26	-27	-29	-30	-32	-33	-34	-36	-35	-36	-36	-36	-37	-37	-37	-36	-36	-36	-35	-34	-32	-31	-30	-26	-20	-20	-17
	MEAN	COMPS	Z I	0	-	-	-	0	-	-	-	-	7	-	-	-	-		-	0	-	7	7	3	4	4	w.	2	2	9	9	2	2	4	4	3	3	4	3	3	7	0	-1	-2
	ROCKET-	SONDE		25	26	27	28	29	30	31	32	33	34	35	.36	37	38	39	04	41	42	43	44	45	46	47	84	64	20	21	52	53	54	55	26	57	58	59	09	61	62	63	64	65

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	DENS.	STD DEV.	1.220	.926	.747	.615	. 539	.454	.384	.334	.308	.281	.254	.231	.214	.192	.173	.165	.154	.138	.126	.115	.103	.091	.081	920.	.067	.062	940.	.042	.037	.032	.029	.026	.023	.021	.045	.015	910.	.014	.013	.011	.010
	PRESS	DEV.	.701	. 599	767.	.439	.398	.360	.328	.300	.276	.253	.231	.212	.192	.176	.160	.145	.130	.116	.104	.093	.082	.073	990.	.058	.052	940.	.038	.034	.032	.028	.025	.023	.021	610.	.018	.015	.015	.013	.012	.011	600.
1969 - 1975	TEMP STD	DEV.	4.1	4.0	3.8	4.0	4.0	9.4	4.5	4.7	9.4	4.3	4.3	4.4	9.4	4.3	4.4	4.1	4.1	4.2	3.8	4.0	4.2	4.4	4.2	4.3	4.1	4.1	3.7	3.8	4.2	9.4	5.0	5.3	5.2	5.7	6.5	6.9	8.9	6.9	7.4	8.1	8.4
	STD	W-E	3.9	5.8	2.0	2.0	5.4	6.1	7.8	6.3	9.9	6.5	8.9	8.7	10.9	9.1	6.7	9.3	4.6	10.1	10.0	12.1	11.9	11.3	13.5	14.1	14.9	14.7	13.0	14.4	15.4	15.5	12.8	13.0	14.2	17.0	15.6	13.9	13.5	15.0	16.4	19.4	22.8
	WIND	S-N	5.6	3.2	5.6	3.3	3.2	9.9	3.5	3.8	8.5	4.0	4.0	4.2	2.1	2.0	5.4	5.9	0.9	6.3	7.0	7.7	0.9	7.8	7.8	7.8	9.5	8.3	8.1	8.9	9.8	8.5	11.1	11.0	11.6	11.7	17.8	11.7	12.2	11.9	13.6	17.3	16.8
	TOTAL	OBSNS	106	126	131	133	132	133	133	135	134	131	135	134	135	133	134	133	135	134	135	134	133	133	133	133	133	131	129	128	126	126	124	119	115	115	113	106	95	06	83	70	53
	MEAN	G/CU M	41.353	35.313	30.191	25.841	22.138	18.975	16.288	14.010	12.051	10.368	8.936	7.697	6.635	5.727	4.940	4.272	3.711	3.219	2.796	2.439	2.130	1.864	1.636	1.438	1.268	1.118	.985	.873	.772	.683	. 605	.535	.473	.419	.366	.326	.288	,255	.224	.198	.175
	TOTAL	OBSNS	102	126	131	133	132	133	133	135	134	131	135	134	135	133	134	133	135	134	135	132	133	133	133	133	133	131	129	128	126	126	124	119	120	115	113	106	95	90	83	70	53
SEPTEMBER	MEAN	MBS	26.500	22.791	19.629	16.914	14.594	12.608	10.890	9.429	8.165	7.082	6.146	5.341	4.651	4.055	3.540	3.097	2.715	2.382	2.093	1.851	1.619	1.428	1.259	1.109	.979	.874	.760	.671	.591	.521	094.	.405	.356	.314	.276	.242	.212	.186	.162	.142	.125
	TOTAL	OBSNS	110	129	134	136	135	136	136	138	137	133	138	137	138	136	137	136	138	137	138	137	136	136	136	136	136	134	132	130	128	128	126	121	117	117	114	107	95	90	83	70	53
1961 -	MEAN	DEG C	8.64-	-48.0	9.94-	-45.0	-43.3	-41.6	-40.1	-38.8	-37.2	-35.2	-33.5	-31.4	-28.9	-26.6	-23.5	-20.8	-18.1	-15.0	-12.0	8.6-	-7.8	-6.1	-5.0	4.4-	-4.1	-3.7	-4.3	-5.3	-6.2	-7.2	-8.6	8.6-	-10.8	-12.1	-13.4	-15.3	-17.4	-19.1	-21.4	-23.1	-24.9
	TOTAL	OBSNS	246	268	275	281	279	282	286	288	288	287	285	289	286	285	287	287	285	282	282	280	277	276	276	273	270	270	267	259	253	247	245	233	225	216	203	183	167	157	142	129	108
	WIND	W-E	8	6-	6-	6-	6-	6-	6-	8	8-	9	9	-7	-	8	8	80	8	-10	6-	-10	-10	6-	6-	8	9	4-	-5	4-	-3	-2	7	0	7	7	4	9	7	80	80	6	12
	MEAN	S-N	1	0	-1	1	-	1	-	7	2	2	0	0	0	0		1	2	1	2	. 7	3	3	4	2	9	. 5	2	2	2	2	5	9	9	9	9	4	4	2	7	1	7
	ROCKET-	SONDE	25	56	27	28	56	30	31	32	33	34	35	36	37	38	39	40	41	42	43	77	45	94	47	48	64	50	51	52	53	54	55	56	57	58	59	09	61	62	63	99	65

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DENS. STD DEV.	1.824	1.548	1.341	1.127	.939	.778	.654	.583	.507	.427	.358	.310	.286	.244	.214	.192	.167	.146	.105	.120	.105	760.	.083	-075	190.	.059	640.	.045	.042	.037	.033	.029	.027	.023	.021	.020	.018	.016	.015	.014	.011
PRESS STD DEV.	1.126	876.	.804	. 688	. 592	.516	464.	.393	.343	.302	.268	.237	. 209	.188	991.	.148	.132	.117	060.	760.	.085	.075	890.	.061	.054	.048	.043	050.	.036	.032	.029	.025	.024	.022	.019	.018	.016	.014	.014	.012	.010
1969 - 1975 TEMP STD DEV.	2.8	3.2	3.4	3.5	3.6	3.3	3.5	3.8	3.6	4.2	4.0	4.1	2.0	4.3	2.0	4.7	4.7	4.7	6.4	4.3	4.4	4.4	4.5	9.4	5.0	8.4	4.8	5.1	5.5	2.6	5.5	5.8	6.1	4.9	6.7	6.9	7.3	7.5	7.9	8.0	7.9
STD W-E	6.5	6.7	7.7	8.2	9.1	10.1	10.9	11.6	12.9	13.6	14.7	16.4	17.0	17.3	18.1	18.7	18.8	18.8	19.3	19.6	19.4	19.7	19.8	50.6	21.7	23.1	24.5	25.1	26.0	26.5	21.5	21.6	22.3	22.1	21.9	22.7	22.8	24.0	25.1	26.1	26.8
WIND DEV.	3.0	3.0	3.5	3.6	3.6	4.0	4.2	4.8	5.4	6.1	5.9	5.8	6.2	6.5	6.7	2.8	6.3	4.9	7.3	8.4	8.1	8.5	8.8	6.7	8.6	8.6	6.6	10.2	6.6	11.6	12.4	12.4	12.3	12.2	13.2	14.9	13.9	15.2	191	17.7	20.1
TOTAL	136	151	155	157	160	191	191	191	191	191	191	162	191	191	162	191	162	162	159	157	157	158	157	157	157	157	154	150	150	120	146	144	137	134	127	120	105	86	84	17	53
MEAN DENSITY G/CU M	40.731	34.763	29.689	25.402	21.762	18.661	16.008	13.738	11.769	10.103	8.682	7.480	6.459	5.533	4.774	4.120	3.561	3.081	2.666	2.325	2.030	1.779	1.562	1.373	1.208	1.066	076.	.832	.737	.651	.577	.511	.451	.399	.352	.311	.274	.243	.214	.189	.166
TOTAL	136	151	155	157	160	161	191	101	191	191	161	162	191	191	162	161	162	162	159	157	157	158	157	157	157	157	154	150	150	150	146	144	137	134	127	120	105	86	84	11	53
OCTOBER MEAN PRESS MBS	25.917	22.268	19.151	16.479	14.183	12.228	10.551	9.120	7.882	6.823	5.916.	5.136	4.466	3.885	3.390	2.959	2.584	2.984	1.984	1.770	1.539	1.356	1.196	1.053	.928	.819	.723	.638	.563	.495	.437	.384	.338	.297	.261	.229	.201	.178	.155	.136	.119
1975 C TOTAL OBSNS	139	153	158	191	163	165	165	165	165	165	165	166	165	165	166	165	166	166	163	161	191	161	160	159	159	159 .	156	152	152	152	148	146	139	136	129	122	107	66	82	. 17	53
1961 - MEAN TEMP DEG C	-51.5	-50.0	-48.4	-47.2	-46.1	6.44-	-43.4	-41.8	-39.8	-37.8	-35.8	-33.9	-31.1	-28.6	-25.8	-22.9	-19.9	-16.9	-13.7	-11.2	-9.0	-7.6	7-9-	-5.9	-5.5	-5.4	-5.8	7.9-	-7.3	-8.4	-9.8	-11.1	-12.3	-13.6	-15.1	-16.5	-17.9	-18.9	-20.2	-21.7	-22.9
TOTAL	286	305	312	318	321	324	326	326	328	328	329	327	324	324	323	324	312	320	315	314	316	313	306	304	300	536	288	283	278	270	797	257	245	240	230	218	195	178	160	141	122
WIND MPS W-E	1	7	7	4	2	2	1	6	11	13	15	16	18	20	20	21	22	23	25	27	. 53	30	32	34	37	39	41	42	77	45	94	47	48	64	20	20	20	64	94	47	41
MEAN COMPS S-N	0	0	-	1	1	1	2	2	2	7	7	2	1	0	0	0	1	1	2		2	5	9	7	&		&	1	00	80	&	7	7	7	7	00	1	7	2	4	3
ROCKET- SONDE	25	56	27	28	29	30	31	32	33	34	35	36	37	38	39	040	41	42	43	44	45	94	47	84	64	20	21	52	53	54	55	26	57	28	59	09	61	62	63	99	65

	DENS.	DEV.	1.558	4.112	3.407	2.932	2.521	2.186	1.885	1.535	1.336	1.154	776.	.838	.730	.619	. 543	987.	.420	.376	.322	.287	.249	.217	.190	.171	.157	.145	.131	.117	.105	.095	.084	.077	.067	090.	.054	640.	770.	.017	910.	.014	.012
		DEV.	.928	2.641	2.233	1.932	1.651	1.414	1.212	1.047	.910	.791	769.	909.	.541	644.	.418	.371	.327	.291	.258	.229	.202	181	.162	.145	.130	.117	104	.092	.082	.073	.064	.057	.051	.045	040	.038	.034	.014	.013	.012	.011
1969 - 1975	_	DEV.	3.4	4.1	4.2	4.4	4.3	3.9	4.1	4.3	8.4	5.1	5.5	9.6	0.9	5.7	5.8	5.9	6.5	6.9	8.9	4.9	6.2	4.9	9.9	6.7	9.9	7.0	6.9	6.5	6.5	13.7	7.2	7.3	7.4	6.9	7.1	15.9	7.5	8.5	4.6	8.6	10.4
	STD	W-E	7.4	8.9	9.6	10.9	10.9	11.4	12.4	12.8	13.4	14.1	13.0	13.3	13.4	12.9	13.1	12.9	13.1	14.0	14.3	15.8	16.2	17.8	19.4	20.1	20.8	22.5	23.0	23.8	24.5	73.7	24.5	23.0	22.9	24.7	26.2	54.9	25.3	27.1	27.3	42.7	41.0
	WIND		4.5	4.7	5.3	5.4	5.9	8.9	8.9	7.0	7.3	6.8	2.6	8.2	8.0	9.6	8.3	7.8	7.9	7.8	8.7	6.1	10.5	10.3	10.3	10.9	11.9	12.6	14.3	15.7	14.8	15.1	15.8	15.3	14.4	14.4	16.6	17.4	16.3	18.0	18.4	21.9	54.9
	TOTAL	OBSINS	118	128	132	132	135	136	137	137	137	137	136	137	133	133	135	133	134	133	132	129	129	128	128	126	125	123	123	122	119	115	114	111	110	106	103	92	84	73	19	54	32
	MEAN	G/CU M	40.120	34.420	29.255	24.980	21.374	18.296	15.673	13.424	11.497	698.6	8.482	7.284	6.259	5.379	4.635	3.998	3.450	2.984	2.585	2.243	1.960	1.714	1.500	1.316	1.154	1.013	.895	.793	.700	.619	. 548	.484	.427	.377	.333	.295	.261	.227	.200	.175	.154
	TOTAL	OBSINS	118	128	132	132	135	136	137	137	137	137	136	137	133	133	135	133	134	133	132	129	129	128	128	126	125	123	123	122	119	115	114	=======================================	110	106	103	92	84	73	61	54	32
NOVEMBER	MEAN	MBS	25.238	21.804	18.696	16.071	13.820	11.896	10.251	8.848	7.637	6.604	5.714	4.955	4.297	3.736	3.257	2.845	2.486	2.177	1.909	1.674	1.475	1.299	1.144	1.006	.885	.778	989.	919.	.534	.470	.414	.364	.320	.281	.247	.218	.191	.166	.146	.128	.111
N 5761	TOTAL	OBSINS	121	131	135	137	139	140	141	141	142	142	142	143	139	139	141	139	140	139	139	136	135	134	134	132	131	129	129	128	125	122	120	116	115	111	107	97	88	11	49	26	34
1961	MEAN	DEG C	-53.9	-52.3	-50.4	0.64-	-47.8	9.94-	-45.1	-43.5	-41.6	-39.9	-38.4	-36.0	-33.8	-31.0	-28.1	-25.2	-22.1	-18.8	-15.7	-13.1	-10.8	-9.0	4.01-	9.9-	-5.7	-5.6	-5.6	-6.8	-7.8	-8.0	-10.0	-11.2	-12.1	-13.3	-14.4	-14.3	-16.7	-18.1	-18.3	-19.0	-20.1
	TOTAL	OBSNS	227	250	257	258	261	262	263	264	566	267	265	267	265	268	268	267	569	268	267	265	797	259	255	255	252	252	251	247	244	238	525	218	212	506	200	178	158	133	112	8	80
	MIND	W-E	6	12	14	16	18	20	23	56	28	31	34	37	04	41	.43	45	47	64	52	54	. 85	09	63	99	69	11	72	74	75	9/	9/	9/	9/	75	75	74	73	11	02	62	61
B.	MEAN	S-N	1	1	7	7	3	٣	4	4	2	2	2	4	4	9	3	3	4	2	9	1	80	10	. =	12	13	17	13	14	14	14	13	13	13	13	12	12	=======================================	11	6	9	6
	ROCKET	SONDE	25	26	27	28	29	30	31	32	33	35	35	36	37	38	39	04	41	42	£ 3	5	45	94	47	848	64	20	51	52	53	54	55	26	57	28	29	9	61	62	63	49	65
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MEAN WIND COMPS MPS S-N W-E	101	4 °	1	13	16	18	22	27	E	35	67	46	64	52	54	26	58	61	99	99	67	89	6 6	22	72	73	71	73	74	74	74	4 5	747	14	75	
TOTAL	120	243	249	546	251	252	254	251	251	252	240	647	248	247	245	245	242	241	239	235	235	234	737	227	221	216	213	208	200	186	182	177	146	131	112	
1961 MEAN TEMP DEG C	-53.9	-51.7	-50.5	-49.1	-47.8	-45.9	-43.8	-41.4	-38.7	-36.3	130.4	22.2	-24.4	-21.2	-17.9	-14.8	-11.3	-8.1	-6.0	1-4-7	-4.3	-3.3	4.5.4	14.0	-5.6	-7.4	-8.6	-9.8	-11.1	-12.8	-14.3	12.	-18.5	-18.8	-21.0	
- 1975 D TOTAL OBSNS	125	142	144	148	148	149	151	150	150	149	17.8	147	145	146	146	146	144	143	144	141	141	139	139	133	131	129	129	127	120	115	113	101	101	75	79	
DECEMBER MEAN PRESS MBS	25.035	18.421	15.803	13.581	11.682	10.064	8.679	7.492	9.476	5.614	4.0.4	3 693	3.224	2.818	2.466	2.162	1.902	1.674	1.475	1.301	1.145	1.010	268.	969	.615	.543	.478	.422	.371	.325	.286	.250	190	167	146	
TOTAL	117	135	137	138	139	140	141	140	140	139	130	138	136	137	137	137	135	134	135	132	132	130	130	125	124	123	123	121	114	109	107	103	2 6	7.2	79	
MEAN DENSITY G/CU M	39.804	29.001	24.744	21.122	18.066	15.444	13.206	11.280	9.638	8.255	6 005	2,000	4.522	3.887	3.373	2.505	2.580	2.206	1.930	1.692	1.487	1.307	1.155	7067	.801	.712	.631	.558	767.	.435	.383	338	260	229	.202	
TOTAL	117	135	137	138	139	140	141	140	140	139	1 20	138	136	137	137	137	135	134	135	132	132	130	130	125	124	123	123	121	114	109	107	103	7 8	72	79	
WIND DEV.	95.0	4.2	6.4	6.1	6.3	6.7	7.8	8.8	9.5	10.1	13.	12.0	11.5	14.7	14.4	14.7	13.9	14.1	15.4	15.5	16.0	16.4	1.71	19.0	18.2	18.6	19.6	20.2	20.2	20.0	19.8	707	20.6	19.4	20.7	
STD	95.1	12.6	14.3	15.9	17.6	18.3	19.6	21.4	21.9	22.1	22.0	21.0	21.6	19.8	19.9	20.0	20.0	20.7	20.0	21.7	22.9	22.9	23.0	26.9	26.4	26.1	28.8	79.7	25.8	79.9	27.4	0.67	26.7	32.8	32.0	
1969 - 1975 TEMP SID DEV.	5.9	3.0	3.5	3.8	4.3	6.4	5.5	5.8	6.8	9.9	7.7		7	9.1	10.2	11.0	11.8	10.9	10.2	9.5	9.6	8.6	1.6	. 6.7	7.7	7.4	7.6	7.5	7.6	7.5	7.5		0 80	6.8	10.8	
PRESS STD DEV.	469.	780	.424	.379	.330	.294	.265	.241	.218	.200	160	146	135	.124	116	.108	101	760.	980.	.078	.073	.067	790.	050	.045	.042	.039	.034	.031	.027	.023	770.	.017	016	.014	
DENS. STD DEV.	1.189	818	.692	.619	.518	.443	.391	.343	.325	.366	276	100	177	.226	140	.134	.121	901.	.094	.085	.078	.072	900	.055	.051	.047	.043	040	.037	.033	.030	770.	.020	.019	.017	

SECTION I PART 2

Vertical profiles of Mean Temperatures and Mean E-W Component Winds at WSMR by the month for 1961 to 1975 are shown in Figures 2 through 25.

ZKM JANUARY TEMPERATURE CELCIUS FIGURE 2 -1- -24 -23 -21 -19 -19 -19 -19 -23 -27 -30 -36 ANOR SE 4 . . . -39 -44 -41 1-48 --49 -51 -52 -54 -55

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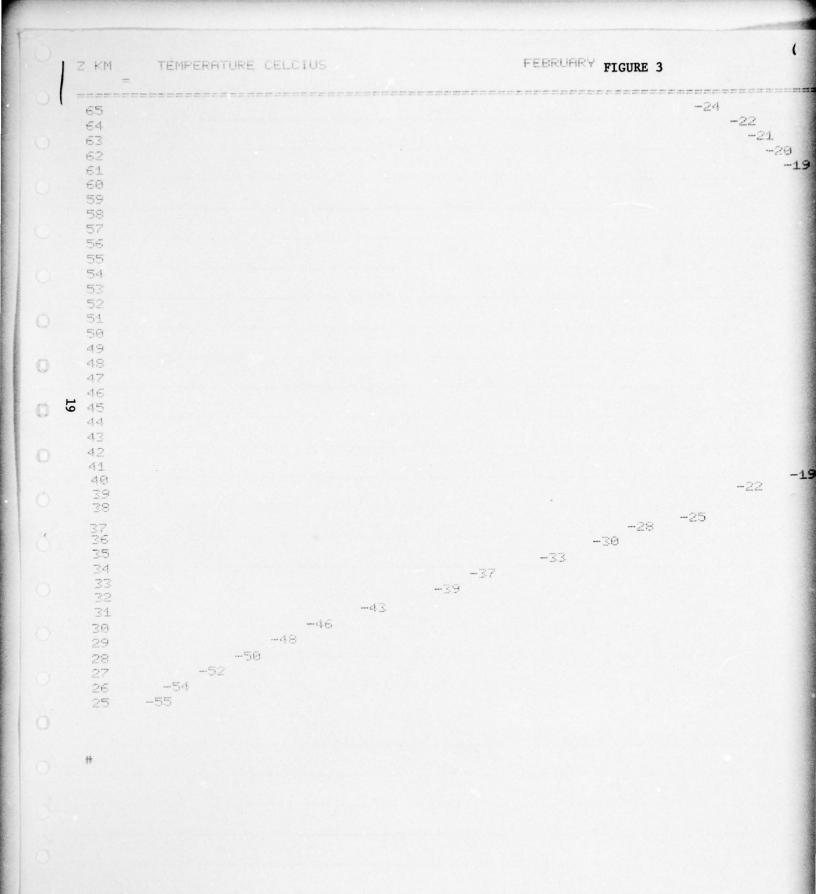
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) ;				Pitterness			-
-				IOMUX CHANNEL		TION	R. ID
	OCTAL	DIF	OCTAL	DIF	OCTAL	DIF	oc
	2622542	-341	146	-45	143540	-14	000
)	2622201	-341	101	-45	143523	-15	000
	2621640	-341	35		143506		000
	2621277	-341		377733	143471	-15	000
)	2620737	-340	377723	-45		-15	000
	2620376	-341	377656	-45	143437	-15	000
	2620035	-341	377611	-45		-15	000
)	2617474	A	377545	-44	143405	-15	000
				IOMUX CHANNEL			R
				UTH			ID
)	OCTAL	DIF	OCTAL	DIF	OCTAL	DIF	oc.
	2247436	-454	221600	-41	117426	-17	006
	2246761			-41			006
)	2246343	-416	221477	-40	117367	-20	006
	2246342	i		-15			006
	2246342	0	221466	4	117372	3	006
)	2246342	Õ				1	
	2246342	Ō	221477		The second secon	1	006
				IOMUX CHANNEL			R
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	2246342	0		O	110727	2	006 (
)	2246342	Õ		0			006
	2246342	Ö	221502	Ō	107513		006
	2246342	Ö	221502	Ō	107205	4	006
	2246342	Õ	221502	0	107033	2	006
	2246342	ō	221502	0	106777	63	006
	2246342	ō	221502	0	107047	.0	006
	2246342		221502	Ō	107143	4	006
	2246342	ō	221502	Ō	107204		006
	2246342	Ō		Ō		3 7	006
	SEQUENCE	NUMBER		OMUX CHANNEL	6		R
				1UTH		110	10
	OCTAL		OCTAL		OCTAL		0C
		0		1423		3	006
	2246342		366053				006
	2246342	Õ	367406	1333	14130	3 2	006 (
	2246342	0	370604	1176	13236		006
	2246342	Ō		1042	12244	2	
	2201220		371646		12344		006
	2246342	Û	372561	713	11452	-672	006
	2246342	Ö Ö	372561 373346	713 565	11452	-672 -672	006 (
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	2246342 2246342 2246342 2246342	0 0 0 0 0	372561 373346 374012 374337 374552	713 565 444 325 213	11452 10560 7670 7000 6112	-672 -672 -670 -670 -666	006 (006 (006 (006 (
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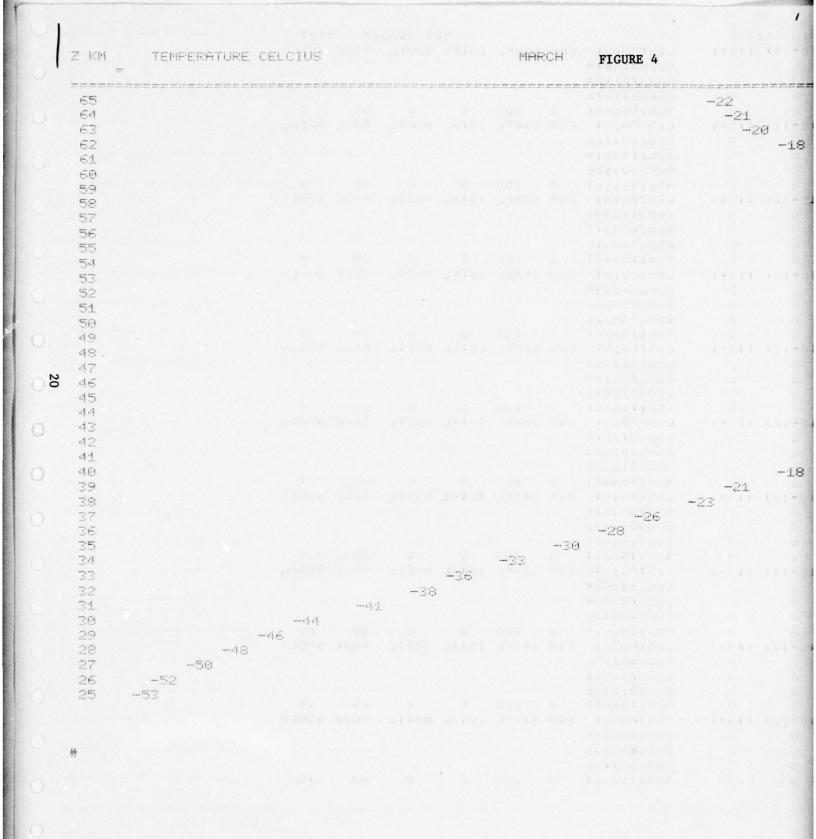
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143405 -15 000 00053 404671712	62	3021 3022	0000
6 RADAH RIZS	0.4	3022	0000
FLEVATION ID MODE TIME	TUIF	SUBSON	ERROR
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117426 -17 006 00127 404772736	62	3688	0000
11/407 -1/ 006 00053 404/73020	62	3689	0000
11/367 -20 006 00127 404/73102	62	3640	0000
117367 U 006 00053 404773164	62	3641	1000
1173/2 3 006 00127 404/73246	62	3692	0000
11/3/3 1 006 30053 404/73330	62	3643	0000
1 17374 1 006 00127 404773412	62	3694	0000
6 RADAR R125	·		
• ELEVATI: • ID MODE TIME	TUIF	SUBSON	ERKOR
OCTAL OCTAL	OCTAL	DEC	RALH
3 006 00127 405001612	62	3758	0000
3 006 00053 405001674	62	3754	0000
107513 -1 006 00127 405001756	62	3760	0000
10/203 202 10 000 00033 103002010	62	3761	0010
107033	62	3762	0010
n 1 000 00033 103002251	62	3763	0010
Tarrend .	62	3764	0010
VL2:1170	62	3765	0000
107204	62	3766	0000
6 _ RADAR RI25	62	3767	0000
.ELEVATIO . ID MODE TIME	TUIF	SUBSON	ERKOR
OCTAL OCTAL OCTAL	OCTAL	DEC	RAEH
15714 3 006 00127 405012436	62	3848	0000
15023 1 006 00053 405012520	62	3849	0000
14130 - 3 006 00127 405012602	62	3850	0000
13236 2 006 00053 405012664	62	3851	0100
12344 2 006 00127 405012746	62	3 g 5 2	0100
11452 -6/2 006 00053 405013030	62	3853	0100
10560 - 672 006 0 0127 405013112	62	3854	0100
76/0 - 6/0 006 00053 405013174	62	3855	0100
7000 -670 006 00127 405013256	62	3856	0100
6112 -666 006 00053 405013340	62	3857	0100
52/3 -66/ 006 00127 405013422	62	3858	0100
4336 -665 006 00053 405013504	62	3859	0100
3451 -665 006 00127 405013546	62	3860	0000
2565 -664 006 00053 405013650	62	3861	0000
1706 -657 006 00127 405013732	62	3862	0000
1150 -536 006 00053 405014014	62	3863	0100
554 -374 006 00127 405014076 314 -240 006 00053 405014160	62	3864	0010
314 -240 006 00053 405014160 174 -120 006 00127 405014242	62 62	3865 3866	0010
132 -42 006 00053 405014324	62	3667	0100
194 -26 006 00127 405014406	62	3868 3868	0000
50 -34 006 00053 405514470	62	7898	0000
10 -40 006 00127 405014552	62	3870	0000
1/7/53 37/7/43 006 00053 405014634	42	3870	0000
377723 -30 006 00127 405014716	62	3872	0010
7///up = 23 006 00053 405015000	62	38/3	0000
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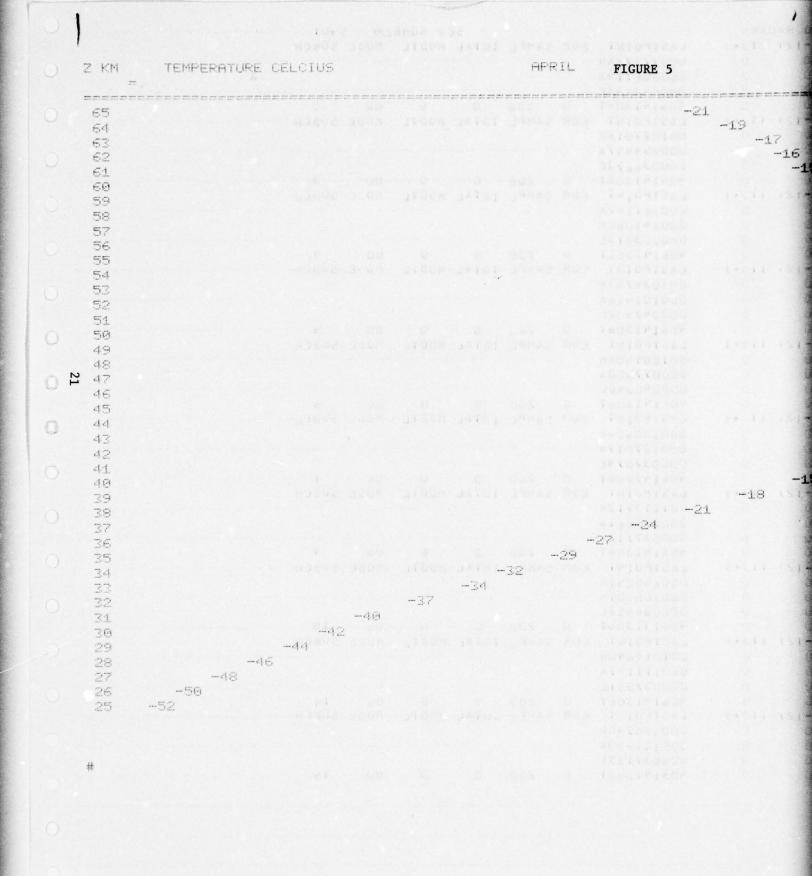
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***SECOND	DIFFERENCE	TABLE	FOR	10 RAD	ARS				- 1
R112				(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTA
RANG	iĒ	0	ō	Ō	0	000631457R			
AZMT	Н	0	0	Ü	0	000370712A			
ELVA	L	0	0	Õ	0	000033747E			
TIME		0	0	Õ	0	4061156661	0	200	0
R122	03 (4-6) (7-91	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTA
RANG	E	0	Ō	Û	0	000660776R			
AZMT	Н	0	0	Õ	0	000274401A			
ELVA	L	0	0	Õ	0	000030655E			
TIME		0	Ö	Õ	0	4061156661	0	200	0
R123	04 (4-6) (7-91	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTA
RANG	E	2	0	Ō	0	000217350R			
AZMT	Н	0	0	Õ	0	00026333IA			
ELVÁ	L	0	0	Õ	0	000042061E			
TIME		0	0	Ō	0	406116444	0	200	0
R124	05 (4-6) (7-91	(10-12)	(13+)	LAST	EOM	SAMPL	IDTA
RANG	E	0	0	O	0	0006			
AZMT	Н	0	0	Ö	0	0000			
ELVA	L	0	0	Ō	0	0000			
TIME		0	0	Õ	0	4061	0	200	0
R125	06 (4-6) (7-91	(10-12)	(13+)	LAST	EOM	SAMPL	IDTA
RANG	E	0	0	0	0	0007			
AZMT	Н	0	0	0	0	0000			
ELVA	L	0	0	Õ	0	0000			
TIME		0	0	ō	0	4061	0	200	0
R127					(13+)	LAST	EOM	SAMPL	IDTA
RANG		0	Ô	0	0	0001			
AZMT		0	0	O	0	0001			
ELVA		0	0	0	0	0000			
TIME		0	0	0	0	4061	0	200	0
R364					(13+)	LAST	EOM	SAMPL	IDTA
RANG		0	0	0	0	0007			
AZMI		0	0	0	0	0000			
ELVA		0	0	Õ	0	0000	-		
TIME		0	0	0	0	4061	-00	200	0
R394			7-91	(10-12)	(13+)	LAST C	EUM	SAMPL	IDIA
RANG		0	0	0		0005			
AZMT		0	0	Õ		0000			
ELVA		0	0	_		000000020		200	
TIME		0	0	0	0	406115666T			
R395						LASTPOINT	EUM	SAMPL	IDIA
RANG	The state of the s	0	Ō	Ō		000650724R			
AZMT ELVA		0	0	Ö Ö		000073160A 000031266E			
TIME	277.	0	0	0	0	4061156661	0	200	0
				article .	(13+)	LASTPOINT		SAMPL	198
RANG		0 (ő			000535064R	2011	SKILL	
AZMI		0	0	Ō	_	000065143A			
ELVA		0	ō	Õ		000030775E			
TIME	-	0	0	Õ	0	406115666T	0	200	0
	SSING FRAM		0	-	U	.001.30001	-		
111	Dated buyer		-						

	*			1				
5					EQ NUME	ER	5201	
3+)	LASTPOINT	EOM	SAMPL	IDTAL	MODTL	MODE	SÜBCH	
0	000631457R						•	
0	000370712A						á	
Ď	000033747E						7	
0	4061156661	0	200	0	0	00	0	
3+1	LASTPOINT	EOM	SAMPL	IDTAL	MODTL	MODE	SUBCH	
)	000660776R				_			
)	000274401A							
)	000030655E							
)	406115666T	0	200	0	0	00	3	
1+)	LASTPOINT				MODIL		SUBCH	
	000217350R							
	00026333TA							
	000042061E							
	4061154427	0	200	0	0	00	4	
+1	LAST		A COLUMN TO THE PARTY OF THE PA		MODTL		SUBCH	
	0006	EOH	SAMEL	IDIAL	MODIL	HODE	3000	
)								
	0000							
	0000		200			0.0		
3+)	4061		200	0	MODTL	00	Suec	
•,	LAST	FOM	SAMPL	IDIAL	MODIL	MUDE	SUBCH	200
	0007							
	0000							
)	0000 G							
		0		0	0	00	. 6	
1+)	LAST	EOM	SAMPL	IDIAL	MODIL	MODE	SUBCH	
) ,	0001							
)	0001							
3	0000							
)	4061	0	7	0	0	00	7	
1+1	LAST	EOM	SAMPL	IDTAL	MODIL	MODE	SUBCH	
)	0007							
)	0000							
)	0000							
)	4061	0	200	0	0	05	9	
1+1	LAST C	EOM	SAMPL	IDTAL	MODTL	MODE	SUBCH	
	0005							
•	0000							
)	0000000236							
)	406115666T	0		0	0	05	10	
+)	LASTPOINT	EOM	SAMPL	IDTAL	MODTL	MODE	SÜBCH	
	000650724R							
	000073160A							
	000031266E							
,	4061156661	0	200	0	0	05	14	
+)	LASTPOINT	EOM	SAMPL	IDTAL	MODTL	MODE	SÜBCH	
	000535064R							
,	000065143A							
	000030775E							
,	4061156661	0	200	0	0	00	15	
	.00	_		A MARTIN MA	-			



TIGURE 5

-21 -19 17 (ST-11) (Y-Y) (STE) -17 -16 -15 -13

2 -10 -9 -8 -6

-4 Till (***) -4 Till (****) -5 -5 -7 -10 -15 -12

-18 (\$1001) (1001) -21

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-1 -1 1

3 0

		E FOR							EQ
8112 00		(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MO
RANGE	0	0	0	0	000771736R				
AZMTH	0	0	0	2	000006114A				
ELVAL	0	0	0	0	000042133E				-
TIME	0	0	0	0	4061413061			0	
122 03	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MO
RANGÉ	1	Ů.	0	0	001027016R				
AZMTH	0	0	Ö	0	000254447A				
ELVAL	0	0	Õ	0	000036673E				
TIME	0	0	Ū	0	4061413061		_	0	
2123 04	(4-6)	(7-4)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MC
RANGE	0	Ô.	Ō	0	000261247R				
AZMTH	0	0	Ō	0	000241066A				
ELVAL	0	0	0	0	000053013E				
TIME	0	0	Õ	0	4061413067	0	200	0	
1124 05	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MC
RANGE	0	Õ	Ó	0	S703R				
AZMTH	0	0	ō	0	416A				
ELVAL	0	0	Ō	0	502E				
TIME	0	Ö	Ö	0	3061	0	200	0	
1125 06	(4-6)	(7-9)	(10-12)	(13+)	INT		SAMPL	IDTAL	MC
RANGE	0	Ö	Ö	0	506R		-		
AZMTH	0	0	Ö	0	500A				
ELVAL	o	ō	ō	0	346E				
TIME	o	0	Ō	0	3061	0	200	0	
127 07	(4-6)	(7-9)	(10-12)	(13+)	INT		SAMPL		ME
RANGE	0	Ö	Ó	0		-			
AZMTH	Ö	0	Õ	0					
ELVAL	a	a	0	0					
TIME	0	Ó	ö	0	CONTRACT	0	200	0	
364 60	(4-6)	(7-9)	(10-12)	(13+)	ESTATE INT		SAMPL	IDTAL	M
RANGE	7 -	0	0	0	712R	20	SAIN L	10175	
AZMTH	0	, 0	Õ		- 561A				
			Õ	0	712E				
ELVAL	0	0	0	0	3061	0	200	0	
TIME	0		(10-13)		Z 101		SAMPL	_	
R394 20	(4-6)	(7-9)	(10-12)	(13+)	?5 I R	EUH	SMALL	IDIAL	71
	0	0	0	0	9 10 IA				
AZMTH	0	0	O Ö	0	32E				
ELVAL	0	0	Ō	0		0	200	0	
TIME 8395 46	0	0	(10=12)	0	1061		200 SAMPL	0	
	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	LUM	SHALL	TOTAL	m.
RANGE	0	0	O ō	0	001014640R				
AZMTH	0	0	0	0	000111141A				
ELVAL	0	0	0	0	000037301E		20.5		10.44
TIME	0	0	0	0	406141306T	0		0	
8393 57	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	FOM	SAMPL	IDIAL	M
RANGE	0	0	0	0	000656740R				
AZMTH	0	0	0	0	000101430A				
	0	0	0	0	000037133E				
ELVAL TIME	0	0	ō	o	406141306T	0	200	0	

```
SEQ NUMBER 5401
LASTPOINT EOM SAMPL IDTAL MODTL MODE SUBCH
000771736R
000006114A
000042133E
406141306T
               200
                     0
LASTPOINT EOM SAMPL IDTAL MODTL
                               MODE SUBCH
001027016R
000254447A
000036673E
406141306T
            0 200 0
                        -0
                              00
LASTPOINT EOM SAMPL IDTAL MODTL
                               MODE SUBCH
000261247R
000241066A
000053013E
406141306T
           0 200 0
                          0
                               00
LASTPOINT EOM SAMPL IDTAL MODTL MODE SUBCH
    5703R
     416A
     502E
            0 200 0 0
     306T
                              00
          EOM SAMPL IDTAL MODTL MODE SUBCH
     INT
     506R
     500A
     346E
               200 0
     306T
                          U
                               00
     INT
          EOM SAMPL IDTAL MODTL MODE SUBCH
     404R
     017A
     D74E
     306T
          0 200 0 0
          EOM SAMPL IDTAL MODTL MODE SUBCH
     INT
     712R
     56 1 A
     712E
               200 0 0
           0
                               05
     306T
     NT
          EOM SAMPL IDTAL MODTL MODE SUBCH
     251R
     DIA
     ,32E
            0 200 0 0 05
     TOOL
          EOM SAMPL IDTAL MODTL MODE SUBCH
LASTPOINT
001014640R
000111141A
000037301E
               200
                     0
                          U
406141306T
                               05
                                     14
LASTPOINT EOM SAMPL IDTAL MODTL MODE SUBCH
000656740R
000101430A
000037133E
406141306T U
               200 0 0
                               00
```

TEMPERATURE CELCIUS FIGURE 6 ZKM _______ -29 -25 -25 -22 +19 -18 -15 -13 -11 -10 -12-15 -21 -24 ACT REVIOUS -34 -- 35 ----41 -43 -45 -47 -49 -50 #

AFILIDE AFILIDE

-18 21

> -2 -4 -9 -12 -15

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		RENCE TABL		10 RAI		C T D O - N T	- 04	e		EQ
R112	00	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDIAL	MC
RANG		0	0	0	0	001132225R				
AZM		0	Ō	O Õ	0	000023004A				
ELV	_	0	0	Ō	0	0000504156		200		
TIM		0	0	1107121	0	4061647261	0		0	
R122		(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EUM	SAMPL	IDIAL	M
RAN		0	0	0	0	001175043R				
AZM		0	0	0	0	000234500A				
ELV		0	0	Ō	0	000045041E		200	_	
IMIT		0	0	(10=12)	(124)	4061647261	0	200	0	
R123	04	(4-6)	(7-9)		(13+)	LASTPOINT 000323117R	EUM	SAMPL	IDIAL	M
RANG		2	0	0	0	000323117R				
AZM		0	0	Ō						
ELV		0	0	Ō	0	000063703E		200	0	
TIME		0	0	0	0	4061647261	50	200	0	
R124		(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EUM	SAMPL	IDIAL	M
RANG	-	0	0	0	0	205316R				
AZM		0	0	Õ	0	115565A				- 000
ELV		0	0	Ŏ	0)52011E				
TIME		0	0	0	0	1647267	0	200	0	
R125	06	(4-6)	(7-9)	(10-12)	(13+)	TPOINT	EUM	SAMPL	IDIAL	M
RANG		0	0	0	0	234460R				
AZM		0	0	Ō	0	114113A				
ELV		0	0	0	0	146746E		200	_	
TIME		0	0	0	0	1647261	0		0	
R127		(4-6)	(7-9)	(10-12)	(13+)	CES POINT	EOM	SAMPL	IDIAL	M
RAN		0	0	0	0	121201K				
AZM		0	0	0	0	14/51UA				- 13
ELV		0	0	0	0	145135E		200		
TIM		C	0	0	0	Entergation 01/201	0	1000		
R364	60	(4-6)	(7-9)	(10-12)	(13+)	Carlo	EUM	SAMPL	IDIAL	М
RANG		0	0	0	0	./33131				- 50
AZM		0	0	0	0	04504A				
ELV		0	0	U	0	- 146322E		200	_	
TIME		0	0	0	0	647261	0	200	0	
R394		(4-6)	(7-9)	(10-12)	(13+)	POINT	LUM	SAMPL	TOTAL	M
RANG		0	0	O õ	0	76622R				
AZM		0	0	0	0	23010A				1
ELV		0	0	Õ	0	44776E		200	0	
TIME			0	(10:13)	0	647261				
R395				(10-12)		CAS (POINT	EUM	SAMPL	TOTAL	-
RANG		0	0	0	0	001160556R				
AZM		0	0	Ö	0	000127106A				
ELV		0	0	Õ	0	000045331E		200		
TIMI		0	0	0	0	4061647261		200		
R393			n ==	(10-12)		LASTPOINT	EUM	SAMPL	IDIAL	14
RANG		0	0	0	0	001000621R				
AZM		0	0	Ō	0	000115723A				
ELV		0	0	0	0	000045361E	-	200		
TIME		0	0	Õ	0	4061647261	0	200	0	19
••M	ISSING	FRAMES =	0							
										-

1 SEQ NUMBER 56UL CASH PULLINE COM SAMPL TOTAL MODIL MODE SUNCH 1991 1 1 2 2 2 2 1 K F DIBLOCATION A 000005U415F 4061647261 () 200 0 (1 1111 LASTPOINT EOM SAMPL IDTAL MODTL MODE SUBCH 001175043R 98023450UA 1-00045041E UU 3 9661647261 O 200 Ü U MUDE SUBCH LASTPOINT EON SAMPL IDTAL MODIL 000323117R 000216563A 0000637036 UΟ 4061647261 200 U U U LASTPOINT EON SAMPL IDTAL MODTLE MODE SUBCH nn 205316R 115565A 352011E 1647261 Ü 200 0 MODE SUBCH TPOINT EOM SAMPL TOTAL MODIL 33446UR 114113A 146746E 200 U 164/26T POINT EUM SAMPL IDTAL MODTL MODE SUBCH (51561R ;4751UA 145135E UU Ü 647261 200 POINT EUM SAMPL IDTAL MODTL MODE SUBCH 17351 3R 04504A 446322E 64726T 200 0 0 05 EOM SAMPL IDTAL MODTL MODE SUBCH POINT 76622R ZJUIUA 44776E 64726T 05 ----10 200 0 LOU (POINT EUM SAMPL IDTAL MODTL MODE SUBCH U01160556R 000127106A 000045331E 200 U U US 9061647261 MODE SUSCH EUM SAMPL IDTAL MODIL LASTPOINT 001000621R 000115723A 000045361E 200 U 99 4061647261

Z KM TEMPERATURE CELCIUS JUNE FIGURE 7 55592 3008 31008 34107 3482 8-25 1070-1213 57-23 2000 -21 7676667167 -19 -16 -14 23 47 -14 -18 -20 -23 -26 -28 -31 -- 23 -35 -38 -40 -42 -45 -47 -49 #

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		ENCE TABL		3 RAI		1			
R113	01	(4-6)	(7-9)	(10-12)	(13+)		FOM	SAMPL	IDI
RAI	IGE	0	0	Ó	0	001016341R			
AZN	ITH	0	0	Õ	0	000025267A			
ELI	/AL	0	0	Õ	0	000032171E			
TIN	1E	0	0	Ō	0	411230544T	0	200	0
R114	02	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDT
RAN	IGE	. 0	0	0	0	000312654R			
AZI	111	0	0	Ö	0	000031325A			
ELV	AL	0	0	Õ	0	000015375E			
TIT	1E	0	0	Ō	0	4112305441	0	200	-
R393	57	(4-6)	(7-9)	(10=12)	(13+)	LASTPOINT	EOM	SAMPL	IDT
RAN	IGE	0	Õ	Ó	0	000345472R			
AZI	1TH	0	0	Õ	0	000042662A			
ELV	AL	0	0	Ō	0	000017627E			
TI	1E	0	0	ō	0	4112305441	0	200	(

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			SI	EQ NUMB	ER	7201		
LASTPOINT	EOM	SAMPL	IDTAL	MODIL	MODE	SUBCH		
001016341R								
000025267A								_
000032171E								1
411230544T	0	200	0	0	00	1	/	
LASTPOINT	EOM	SAMPL	IDTAL	MODTL	MODE	SUBCH		
000312654R								
000031325A								
000015375E								
4112305441	0	200	0	0	00	2		
LASTPOINT	EOM	SAMPL	IDTAL	MODTL	MODE	SUBCH		
000345472R						-		
000042662A								
000017627E								
4112305441	0	200	0	0	00	15		

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Z KM =	TEMPERATURE CE	ELCIUS				JUL		FIGURE 8	
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TGURE 8

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SECOND				10 RAD					5
R112				(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL
RANG		0	0	0	0	002234406R			
AZMT		0	0	0	0	000137157A			
ELVA		0	0	O .	0	000116746E			
TIME		0	0	0	0	4063520661	0	200	0
	03	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL
RANG	THE RESERVE OF THE PARTY OF THE	0	0	0	0	002341243R			
AZMT		0	0	0	0	000075300A			
ELVA		0	3	0	0	000111653E			
TIME		0	0	0	0	406352066T	0	200	0
	04	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL
RANG	The state of the s	2	0	0	0	000636146R			
AZMT		0	0	0	0	000042200A			
ELVA		0	0	0	0	000146515E			
TIME		0	0	0	0	4063520661	0	200	0
		(4-6)	(7-9)	(10-12)	(13+,	' STPOINT	EOM	SAMPL	IDTAL
RANG		0	0	0	0	2362464R			
AZMT		0	0	Õ	0	1231321A			
ELVA		0	0	0	0	1126021E			
TIME		0	0	Õ	0		0	200	0
		(4-6)	(7-9)	(10=12)	(134		EOM	SAMPL	IDTAL
RANG		0	Ō	0	0				
AZMT		0	0	Ō	0	1227276A			
ELVA	L	0	0	Õ	0				
TIME		0	0	Ö	O CHARLE		0	200	0
R127	07	(4-6)	17-91	(10-12)	(134 Canal	STPOINT	EOM	SAMPL	IDTAL
RANG	Ē	2	0	0	0	1321041R			
AZMT	H	0	0	Ö	0)313247A			
ELVA	L	0	0	Õ	O SECOND)112261E			
TIME		0	0	Ō	0	352066T	0	200	0
R364	60	(4-6)	(7-9)	(10-12)	(13+	TPOINT	EOM	SAMPL	IDTAL
RANG	E	0	Õ	ō ·	0	2532204R			
AZMT	Н	0	0	Ō	0	1206355A			
ELVA	L	0	0	Ö	0)120060E			
TIME		0	0	Õ	0	352066T	0	200	0
R394	20	(4-6)	(7-9)	(10-12)	(13+	STPOINT	EOM	SAMPL	IDTAL
RANG	E	0	0	0	0	1747446R			
AZMT	Н	0	0	Õ	0	1242651A			
ELVA	L	0	0	Ō	0	1114651E			
TIME		0	0	0		106352066T			
R395	46	(4-6)	(7-9)	(10-12)	(13+)		EOM	SAMPL	IDTAL
RANG	E	0	0	0	0	002310017R			
AZMT	Н	0	0	0	0	000252765A			
ELVA	L	0	0	Õ	0	000112760E			
TIME		0	Ō	Õ	0	4063520661		200	
R393	57	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL
RANG	E	0	Ô.	0	0	001753755R			
AZMT	Н	0	0	õ	0	000230552A			
ELVA	L	0	0	Ō	0	000121374E			
TIME		0	0	Ō	0	4063520661	0	200	0
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	LASTPOINT	EOM	SAMPL	IDTAL	MODTL	MODE	SÜBCH	
	002234406R							
	000137157A							2
	000116746E							
	406352066T		200				0	
	LASTPOINT	EOM	SAMPL	IDTAL	MODIL	MODE	SUBCH	
	002341243R							
- (000075300A							
(000111653E							E
	4063520661	0	200	0	0	00	3	
1	LASTPOINT	EOM	SAMPL	IDTAL	MODTL	MODE	SUBCH	
(000636146R							
(000042200A							
(000146515E							
1	406352066T	0	200	0	0	00	4	
	STPOINT	EOM		IDTAL	MODTL	MODE	SUBCH	
	2362464R						*	
	1231321A							
	1126021E							
	5352066T	0	200	0	0	00	5	
	STPOINT						SUBCH	
E CONTRACTOR	2436243R						1000.	
	1227276A							
	1116636E							
Ham	352066T	0	200	0	0	00	6	
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ARLAN .	1321041R		3				3.00	
Canada	1313247A							
PARTY AND THE PA)112261E							
	352066T	0	200	0	0	00	7	
200	TPOINT				MODTL		SUBCH	
	2532204R	2011	3 Mill L	IDIAL	110016	11002	30001	
	1206355A							
V.5684)120060E							
	352066T	0	200	0	0	05	9	
3	STPOINT		The state of the s	-		1000		
	747446R	2011	SAME	IDIAL	HOUTE	HODE	SOBCH	
	1242651A							
)114651E							
	1114651E	0	200	0	0	05	10	
				1000	MODTL		SÜBCH	
	LASTPOINT	EUM	SAMPL	TOTAL	MODIL	MODE	SOBCH	
	002310017R							
	000252765A							
	000112760E	244				05		
	406352066T	0		0	0	05	14	
	LASTPOINT	EOM	SAMPL	IDIAL	MODTL	MODE	SORCH	
	001753755R							
	000230552A							
	000121374E							
	406352066T	0	200	0	0	00	15	

AUGUST FIGURE 9 Z KM TEMPERATURE CELCIUS × 1248 -23 -21 -18 CASICOLAT SOR SERVICENT MODE SAPER 25 47 46 -20 -22 -25 -28 -30 -32 -34 -36 -38 -48 -42 -44 -45 -47 -48 -50

FIGURE 9

-26 -25 -23 -21 -18 -15 -11 -10 -9 -7 -13 -6 -6 -5 -5 -5 -7 -8 -9 -12 -14

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Called the source of the season property

SECOND D										EQ
R113 () 1	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	M
RANGE		0	Ö	0	0	001304000R				-
AZMTH	1	0	0	ā	a	000051570A				
ELVAL		0	Ü	ō	0	00004373IE				
TIME		0	0	ō	0	4112541641	0	200	0	
R114 (02	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	1
RANGE		0	Ô	Ó	0	000420325R				
AZMTH	1	0	0	Ö	0	000042200A				
ELVAL		0	0	Ō	0	000022145E				
TIME		0	0	Ō	0	411254164T	0	200	0	
R393 5	57	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	1
RANGE		0	Ō	Ö	0	000467351R				
AZMTH	1	0	0	0	0	000057175A				
ELVAL		0	0	Õ	Ö	000025535E				
TIME		0	Ō	ō	0	4112541641	0	200	0	







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FIGURE 10

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SECOND				3 RA						EQ
R113	01	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MO
RAN	IGÉ	0	Õ	0	0	001571441R				
AZM	TH	0	0	Õ	0	000075716A				
ELV	AL	0	0	Ö	0	000055305E				- 10
TIM	1E	0	0	Õ	0	4112776041	0	200	0	
R114	02	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	HO
RAN	IGË	0	Ô	O	0	000525770R				
AZM	TH	0	0	Õ	0	000053034A				
ELV	AL	0	Ō	Ō	0	000026425E				
TIM	E	0	0	Õ	0	4112776041	0	200	0	
R393	57	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MO
RAN	IGE	0	0 ~	0	0	000611253R				
AZM	TH	0	0	Ō	0	000073524A				
ELV	AL	0	Ō	Õ	0	000033560E				
TIM	E	0	0	Ō	0	411277604T	0	200	0	
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				(
			5	EQ NUMB	ER	7601	
LASTPOINT	EOM	SAMPL	IDTAL	MODTL	MODE	SOBCH	
001571441R						-	
000075716A							
000055305E							
4112776041	0	200	0	0	00	1	
LASTPOINT	EOM	SAMPL	IDTAL	MODTL	MODE	SUBCH	
000525770R							9
000053034A							
000026425E							
4112776041	0	200	0	0	00	2	
LASTPOINT	EOM	SAMPL	IDTAL	MODTL	MODE	SUBCH	
000611253R						-	
000073524A							
000033560E							
411277604T	0	200	0	0	00	15	
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TEMPERATURE CELCIUS

Z KM

OCTOBER FIGURE 11

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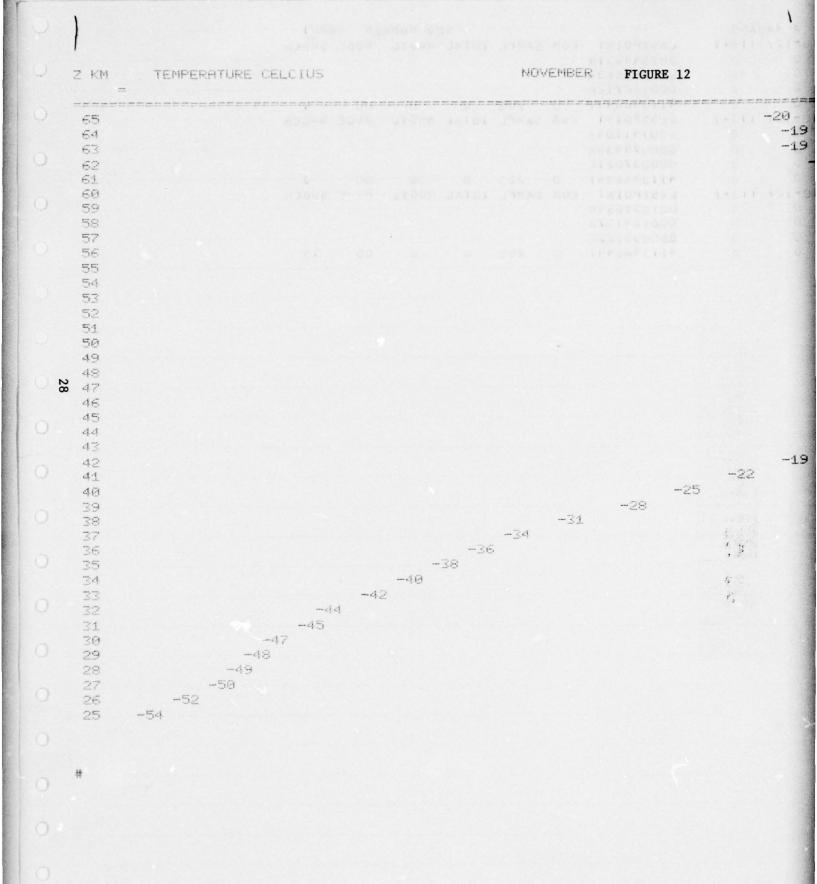
B. Chr. S. J.

SECOND DIFFER			3 RAI						EQN
R113 01	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MOD
RANGE	0	0	Ö	0	002057074R				
AZMTH	0	0	Õ	0	000122251A				
ELVAL	0	0	Ö	0	000067036E				-
TIME	0	0	Õ	0	4113232241	0	200	0	0
R114 U2	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MOD
RANGE	0	Ō	Û	0	000633433R				
AZMTH	0	0	Õ	0	000063652A				
ELVAL	0	0	Õ	0	000032557E				
TIME	0	0	Ũ	0	4113232241	0	200	0	•
R393 57	(4-6)	(7 - 9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MOD
RANGE	0	Õ	Ū	0	000733161R				-
AZMTH	0	0	Ö	0	00010776 LA				
ELVAL	0	0	0	0	000041740E				-
TIME	0	ñ	ñ	0	4113232241	a	200	0	•

RAD	ARS				S	EQ NUMB	ER	7801		
12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MODTL	MODE	SÜBCH		
	0	002057074R								
	0	000122251A								
	0	000067036E					-			
	0	4113232241	0	200	0	0	00	1	2	
12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MODTL	MODE	SUBCH		
	0	000633433R								
	0	000063652A								
	0	000032557E								
	0	4113232241	0	200	0	0	-00	2		
121	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MODTL	MODE	SUBCH		
	0	000733161R						-		
	0	00010776 TA								
	0	000041740E								
	0	411323224T	0	200	0	0	00	15		
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***SECOND	DIFFER	ENCE TABL	E FOR	3 RA	DARS				51	EQ
R113	01	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MO
RANG	Ē	0	Ö	Ô	0	002344531R				
AZMT	Н	0	0	Ō	0	000146563A				
ELVA	L	0	0	Ü	0	000100712E				-
TIME		0	0	Õ	0	4113466441	0	200	0	
R114	02	(4-6)	(7-9)	(10-12)	(13+1	LASTPOINT	EOM	SAMPL	IDTAL	MO
RANG	E	0	Ō	Û	0	000741105R				
AZMI	Н	0	0	Ō	0	000074435A				
ELVA	L	0	0	ō	0	000037021E				
TIME		0	0	Õ	0	4113466441	0	200	0	
R393	57	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MO
RANG	E	0	0	0	0	001055054R				
AZMT	Н	0	0	0	0	000124157A				
ELVA	L	0	O	Õ	0	000050222E				
TIME		0	0	Õ	0	4113466441	0	200	0	
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002344531R 000146563A							
000100712E						2	
4113466441	0		0	0	00	1	
LASTPOINT 000741105R	EUM	SAMPL	IDIAL	MODTL	MODE	SUBCH	
000074435A							*
000037021E	0	200	0	0	00		
LASTPOINT	EOM			MODTL		SUBCH	
001055054R 000124157A							
000050222E							
4113466441	ō	200	0	ō	00	15	

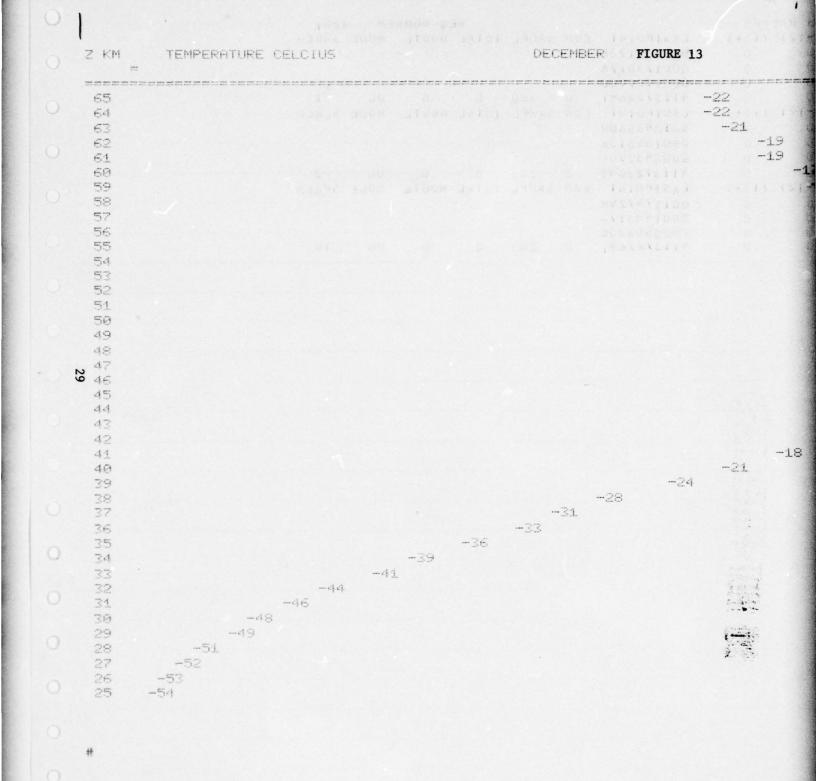


FIGURE 13

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SECON	DIFFER	RENCE TABL	E FOR	3 RAI	DARS				SI	EQ NU
R113	01	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MODT
RAI	NGE	0	Ö	Ō	0	002632170R				
AZI	HTH	0	0	Ö	0	000173017A				
EL	VAL	0	0	Ö	0	000112776E				
TI	ME	0	0	Ö	0	4113722641	0	200	0	0
R114	02	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MODT
RAI	NGE	0	Ō	Ò	0	001046560R				
AZ	MTH	0	0	õ	0	000105313A				
EL	VAL	0	0	ō	0	000043370E				
T1	ME	0	Ō	Õ	0	4113722641	0	200	0	0
R393	57	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MODT
RA	NGE	0	ō	Ô	0	001176725R				
AZI	мтн	0	0	0	0	000140317A				
EL	VAL	0	0	Ō	0	000056520E				
711	ME	0	0	0	0	4113722647	0	200	0	0
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Z KM E-W COMPONENT WINDS MPS +E -W
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R1	SECOND DIFFE 122 03	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT 001412450R	EOM SAUPL	IDTAL
	MEMTH	0	0		0	000136115A		
	ELVAL	0	0	0	0	090126001E		
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Z KM E-W COMPONENT WINDS MPS +E -W FEERUARY FIGURE 15 65 -66 64 -66 63 -67 62 -67 61 -64 -60 -58 -54 -52 -51 -49 -49 -47 -45 51 -44 -43 -42 -40 -38 -35 -32 -30 -28 -36 -25 -25 -24 -22 -21 34

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LASTPOINT 001572342R	ЕОМ	SAMPL	SE	Q NUME	BER 11	SUBCH			_ 0
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Z KM E-W COMPONENT WINDS MPS +E -W
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MARCH FIGURE 16

24 -23 -21 -19 -16

-13 -12 -10 -8 -7 -5 -4 -3

1	R122 03	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MODT
	PINGE	0	0	^	0	001752237R				
	,_MTH	0	0		0	000115412A				
	ELVAL	0	0	0	0	000135405E				
	TIME	0	0	0	e	427104762T	0	200	0	0

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LASTPOINT	ЕОМ	SAMPL	IDTAL	MODTL	BER 11	1201 SUBCH				_ 0
001752237R 000115412A 000135405E		-()				()				
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Z KM E-W COMPONENT WINDS MPS +E -W APRIL FIGURE 17 65 64 63 62 61 60 59 -7 58 -7 57 56 55 54 --9 53 -10 52 -11 51 50 -11 -13 49 -13 48 -14 47 -14 -14 46 45 -14 44 -14 43 -14 42 -14 41 -14 40 -15 -15 39 38 -17 36 36 35 34 -17 -17 -16 -14 -13 33 -10 -9 31 Sealer S 30 29 28 27 26

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R122 03	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL		
NGE	0	0	•	0	002132127R				
2MTH	0	0		0	000105146A		-		
ELVAL	0	0	0	0	000141170E				
TIME	0	0	0	0	427051342T	n	200	0	0
**MISSING F	RAMES =	0							

SEQ NUMBER 11001 LASTPOINT EOM SAMPL IDTAL MODTL MODE SUBCH 002132127R	- 0
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	R122 03	(4-6) (7-9)	(10-12) (13+)	LASTPOINT 002651560R	EOM	SAMPL	IDTAL	MODIL
1	2MTH	0 0	-0	0	0000542024		-(0)		
1	ELVAL	0 0	0	* 0	000154414E				
	TIME **MISSING FRA	$0 \qquad 0$ $MES = 0$	0	0	426766662T	0	200	0	0

LASTPOINT 002651560R 000054202A 000154414E	ЕОМ	SAMPL	S IDTAL	EG NUM MODTL	BER 10 MODE	401 SUBCH			A Parkers (Assum)	O
#26765652T	0	200	0	0	0.0	3		2	_	0
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JUNE FIGURE 19 Z KM E-W COMPONENT WINDS MPS +E -W 35 50 26 29 55 54 34 / 26 - 26 1 25 10 X AXIS OFF PAGE TO LEFT

R122 03	(4-5)	(7-9)	(10-12)	(13+)	LASTPOINT	FOM	SAMP	IDTAL	MOD
TINGE	0	0	,10,12,	0	003031444R	20,-1	JAN. L	101	1400
N_MTH	0	0		0	000043721A				
ELVAL	0	0	. 0	0	000160067E				
TIME	0	0	0	0	426743242T	0	200	0	(

SEQ NUMBER 10201 LASTPOINT EOM SAMPL IDTAL MODTL MODE SUBCH 003031444R 000043721A 000160067E 426743242T 0 200 0 0 00 3	600
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Z KM E-W COMPONENT WINDS MPS +E -W JULY FIGURE 20 36 52 1.7 X AXIS OFF PAGE TO LEFT

R122 03	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EOM	SAMPL	IDTAL	MODTE
NGE	0	0	0	0	003211331R		7		
NCMTH	0	0		0	000033464A				
ELVAL	0	0	0	0	000163517E				
TIME	0	0	0	0	426717622T	0	200	0	0

.

SEQ NUMBER 10001
LASTPOINT EOM SAMPL IDTAL MODTL MODE SUBCH
003211331R
000033464A
000163517E
426717622T 0 200 0 0 00 3

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AUGUST FIGURE 21

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100	R122 03	(4-6)	(7-9)	(10-12)	(13+)	LASTPOINT	EDM	SAMPL	IDTAL A
	NGE	0	0		0	003371205R			
Ī	MTH	0	0		0	000023222A			
	ELVAL	0	0	0	0	000167703E			
	TIME	0	0	0	0	426674202T	0	200	0
	**MISSING FF	RAMES =	0						

SEQ NUMBER 9801	0
LASTPOINT EOM SAMPL IDTAL MODTL MODE SUBCH 003371205R	
000023222A 000167703E	0
426674202T 0 200 0 0 00 3	-
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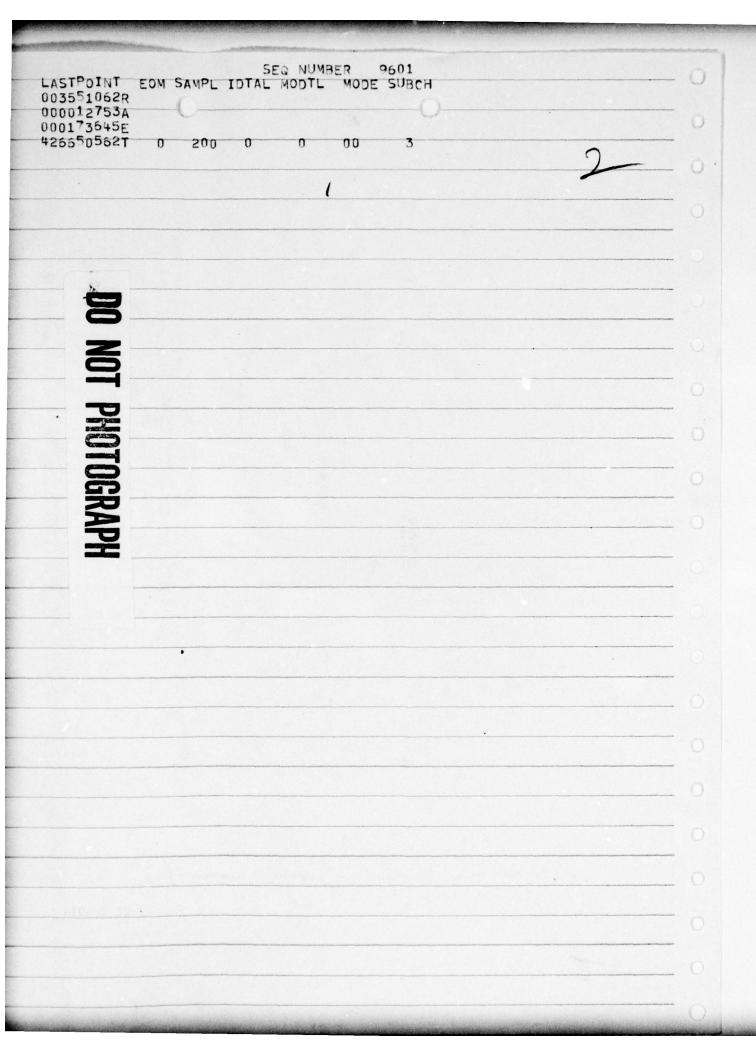
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R122 03	(4-0)	11-91	(10-12)	(13+)	LASTPOINT	EUM	SAMPL	IDIAL	MI
NGE	0	0	^	0	003551062R				
MTH.	0	0		0	000012753A		V		-
ELVAL	0	0	0	0	000173645E				
 TIME	0	0	0	0	426650562T	0	200	0	
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Z KM E-W COMPONENT WINDS MPS +E -W
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Z KM E-N COMPONENT WINDS MPS +E -W NOVEMBER FIGURE 24 -61 -62 -78 -71 -74 -75 -75 -76 -76 -76 -76 -75 -74 -72 -71 -69 -66 -75 52 51 -53 .8 -58 -54 -52 -49 -47 -45 --50 -43 -41 --40 --37 --34 --31 -41 33 32 31 30 -28

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O

	27	COMPONENT WINDS M			FIGURE 25
65	-80				
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63		-75			
62		-74			
61		-74			
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FIGURE 25

-39 -35

-31 -27 -18 -16 -13 -11 -8 -11 -10

SECTION II PART 1

STRATOSPHERIC MODEL OF CLIMATOLOGICAL PARAMETERS OVER WSMR

This section presents models of the climatological data presented in Section I of this report. Stratospheric temperature, density, pressure, and wind components are modeled from 25-65 km on a Julian day basis. Following the presentation of the model is a detailed analysis of several spring and autumn wind crossover patterns. The modeling of the stratospheric parameters has been basically approached from a best fit point of view.

The model for the stratospheric wind is divided into two sections (North-South components and East-West components). The reader should note that the sign convention is the opposite to that utilized in Section I of this report, i.e., the model assigns + to N,E and - to W,S winds. A copy of the E-W model has been included showing nicely the spring and autumn crossovers (Table 13).

The essential equations and routines used for the E-W circulation model are presented briefly below. Essentially they consist of a best fit trigonometric function.

- 0110 PRINT "INPUT JULIAN DAY"
- 0130 INPUT X
- 0132 PRINT
- 0170 PRINT "INPUT Z IN KM"
- 0190 INPUT Z
- 0191 PRINT
- 0230 LET B=45
- 0250 LET A=B-X
- 0270 IF X<45 THEN LET A=0
- 0290 IF X>315 THEN LET A=270
- 0310 LET H1=-(2/3)*Z+148.33
- 0330 LET H2=-(2/3)*Z+298.33
- 0350 IF X<165 THEN LET D=-(70/45)*Z+361.111
- 0370 IF X=>165 THEN LET D=-Z+350
- 0390 IF X>165 THEN IF X<195 THEN LET A+(270/360)*180
- 0410 LET J=1.71428*Z-41.4284
- 0430 IF Z<30 THEN LET J=5
- 0450 LET Y=-J*COS((A*360)/(D*57.295))
- 0470 LET Y-INT(Y)

E-W WIND COMPONENT MODEL TABLE 13

B. H. BTHD. ONE CHOOL UPDED TOWN 17												
DAY				HEIGH	TS IN E							
	20	25	30	35	40	45	50	55	60	65		
1	5-	5-	10-	19-	28-	36-	45-	53-	62-	70-		
6	5-	5-	10-	19-	28-	36- 36-	45-	53-	62-	70- 70-		
11 16	5- 5-	5- 5-	10-	19- 19-	28- 28-	36-	45-	53-	62-	70-		
21	5-	5-	10-	19-	28-	36-	45-	53-	62-	70-		
26	5-	5-	10-	19-	28-	36-	45-	53-	62-	70-		
31	5-	5-	10-	19-	28-	36-	45-	53-	62-	70-		
36	5-	5-	10-	19-	28-	36-	45-	53-	62-	70-		
41	5-	5-	10-	19-	28- 28-	36- 36-	45-	53- 53-	62- 62-	70- 70-		
51	5-	5-	10-	19-	27-	36-	44-	53-	61-	70-		
56	5-	5-	10-	19-	27-	35-	43-	52-	60-	68-		
61	5-	5-	10-	18-	26-	34-	42-	50-	58-	65-		
66	5-	5-	10-	17-	25-	33-	40-	47-	55-	62-		
71	5-	5-	9-	16-	24-	31-	38- 35-	44-	51- 46-	57- 52-		
76 81	5- 4-	5-	9- 8-	15- 14-	22-	29- 26-	31-	37-	41-	46-		
86	4-	4-	7-	13-	18-	23-	28-	32-	36-	39-		
91	4-	4-	7-	11-	16-	20-	24-	27-	29-	32-		
96	3-	3-	6-	10-	13-	17-	19-	21-	23-	24-		
101	3-	3-	5-	8-	11-	13-	15-	16-	16-	16-		
106 111	2-	2-	4-	6-	8-	9-	10-	10-	9-	7-		
116	2-	1-	2-	3-	3-	2-	ó	2	5	10		
121	1-	1-	1-	1-	ō	2	5	8	12	18		
126	1-	0	0	1	3	6	9	14	19	26		
131	0	0	1	3	6	10	14	20	26	34		
136 141	0	1	2 3	5 7	9	13 17	19 23	25 30	32 38	41		
146	i	i	4	8	14	20	27	35	44	53		
151	2		5	10	16	23	31	39	48	58		
156	2	2 2 3	6	12	18	26	34	43	• 52	62		
161	2	3	6	13	20	28	37	46	56	66		
166 171	4	4	8	16	24	33	42	50	59	69		
176	4	4	8	16 16	24	33 33	42	50 50	59 59	69		
181	4	4	8	16	24	33	42	50	59	69		
186	4	4	8	16	24	33	42	50	59	69		
191	4	4	8	16	24	33	42	50 .	59	69		
196	4	4	9	18	27	35	44	52	60	68		
201 206	4	4 4 4	9	18 18	27 26	35 35	43	51 50	59 57	66 64		
211	4	4	9 9	18	26	34	41	48	55	60		
216	4	4	9	17	25	33	40	46	51	56		
221	4	4	9	17	24	31	37	43	48	51		
226	4	4	9	16	23	29	35	. 39	43	46		
231 236	4	4	8	15 14	21 20	27 25	32 28	36 31	38 33	40 33		
241	4	3	7	13	18	22	25	27	27	26		
246	3	3	6	12	16	19	21	22	21	19		
251	3	3	6	10	13	16	17	16	15	11		
256	3	2 2 2	5	8 7 5 3	11	12	12	11	8	4		
261 266	2 2	2	4	7	8	9 5	8	5	1 5-	12-		
271	1	1	3 2	3	3	2	1-	6-	12-	19-		
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281	1	0	0	0	2-	6-	11-	17-	24-	33-		
286	0	0	1-	2-	5-	9-	15-	22-	30-	40-		
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301	1-	2-	4-	8-	13-	16- 20-	27-	36-	46-	57-		
306	2-	2-	5-	9-	15-	23-	31-	40-	50-	61-		
311	2-	3-	5-	11-	18-	25-	34-	44-	54-	64-		
316	3-	3-	6-	12-	19-	27-	36-	46-	56-	67-		
321	3-	3-	6-	12-	19-	27-	36-	46-	56-	67-		
326 331	3- 3-	3- 3-	6-	12- 12-	19- 19-	27- 27-	36- 36-	46-	56- 56-	67- 67-		
336	3-	3-	6-	12-	19-	27-	36-	46-	56-	67-		
341	3-	3-	6-	12-	19-	27-	36-	46-	56-	67-		
346	3-	3-	6-	12-	19-	27-	36-	46-	56-	67-		
351	3-	3-	6-	12-	19-	27-	36-	46-	56-	67-		
356	3-	3-	6-	12-	19-	27-	36-	46-	56-	67-		
361	3-	3-	6-	12-	19-	27-	36-	46-	56-	67-		

The E-W profiles fall into generally three major categories based on the slope of the curves. Type 1 - for strong well established easterly or westerly flow, the curves are nearly linear (Figure 14). Type 2 - for flow that still is predominately strong easterly or westerly, but is beginning to suggest a slowdown above 50 km. The profile suggests a hook configuration (Figure 16). Type 3 - this profile is strongly parabolic and occurs during the actual spring and fall turnovers (Figure 17).

The approach for the N-S circulation model was a best fit cubic polynomial with an additional logarithmic term with the following sign convention:

at Z = 25km Y = 1 mps where Y is N/S component in mps at Z = 65km

$$Y_{65}(D) = -63.597516_{2} - 6.136 * D$$
 $-.0057 * D^{2} + 34.3045 * 1n(D)$
 $+.000004275 * D^{3}$
 $+1.231017 * D * 1n(D)$

$$Y_Z(D) = \frac{Z - 25 (Y_{65}(D) - 1) + 40}{40}$$

where: Z is altitude in km

Y, (D) = N/S wind in mps at Z km at Day "D"

Y₆₅(D) is N/S wind in mps at Day "D" at 65km

The approach is to best fit the wind in altitude then linearally interploate for time.

Both density and pressure being more conservative were best fit exponentially in height and then linearally interploated in time. The equations are as follows.

DENSITY MODEL

Exponential spatial fit linearally interpolated temporal fit

$$P = e^{(J - .143 Z)} + f$$

Z in km

for
$$1 \le \text{Day} \le 182$$
, $J = \frac{(D-1) (0.13)}{181} + 7.17$
for $82 \le \text{Day} \le 365$ $J = \frac{(D-182) (-0.13)}{183} + 7.3$

f = 3.3 for Jan, 25km only

PRESSURE MODEL

Exponential spatial best fit linearally interpolated temporally

$$P = e^{(J - .13Z)} + f$$

 $f = 1.2$ 25km only
for $1 \le Day \le 182$ $J = \frac{(D-1) (.0)}{181}$

for
$$1 \le \text{Day} \le 182$$
 $J = \frac{(D-1)(.05)}{181} + 6.45$
for $182 \le \text{Day} \le 365$ $J = \frac{(D-182)(-.05)}{183} + 6.50$

Novlan modeled temperature from another best fit point of view. Temperature was best fit to a cubic polynomial in altitude with a term added then linearally interpolated for time. Results are good within 2 to 3°C. The equations are presented below:

TEMPERATURE MODEL

$$T_1$$
 (Jan) $C^{\circ} = -2400.59756 - 2593.055 Z$
 $-10.37 Z^2 + .0216933 Z^3$
 $+6092.022 \ln(Z)$
 $+665.3986 Z \ln(Z)$

T₂ (June)
$$C^{\circ} = -3799.172 - 2260.56647 Z_{-7.78677} Z^2 + .0216933 Z^3 +6111.4755 ln(Z) +560.69812 Z ln(Z)$$

for
$$1 \le D \le 182$$

$$\frac{(T_2 - T_1) (D-1)}{181} + T_1 = T$$
 for $182 \le D \le 365$
$$\frac{(T_1 - T_2) (D-182)}{183} + T_2 = T$$

where T is in C°

McCullough utilized a least squares approach of a limited harmonic analysis method to model the stratospheric temperature. The model produces accuracies less than 1°C; however, as seen below, the model is lengthly and requires linear interpolation between 5km height increments. The equations are as follows:

```
LIST
0005 LET X=1
0010 PRINT
0018 LET Y=-51.913-2.88*COS(6.28*X/365)-.725*SIN(6.28*X/365)
0020 LET Y=Y-.239*COS(4*3.14*X/365)-.323*SIN(4*3.14*X/365)
0 030 LET A=INT(Y) 25KM
0040 LET Y=43.525-8.751*COS(6.28*X/365)+.434*SIN(6.28*X/365)
0050 LET Y=Y-.5608*COS(4*3.14*X/365)+.1981*SIN(4*3.14*X/365)
0060 LET Y=Y- .0992*COS(6*3.14*X/365)+.097*SIN(6*3.14*X/365)
0070 LET Y=Y+.263*COS(8*3.14*X/365)-.268*SIN(8*3.14*X/365)
0 080 LET B=INT(Y) 30KM
0090 LET Y=-32.517-3.183*COS(6.28*X/365)+3.014*SIN(6.28*X/365)
0100 LET Y=Y-.3416*COS(4*3.14*X/365)+.757*SIN(4*3.14*X/365)
0110 LET Y=Y-.3745*COS(6*3.14*X/365)+.526*SIN(6*3.14*X/365)
0120 LET Y=Y-.1*COS(8*3.14*X/365)-.4861*SIN(8*3.14*X/365)
0130 LET Y=Y-.302*COS(31.4*x/365)-.588*SIN(31.4*x/365)
0 140 LET C=INT(Y) 35KM
0150 LET Y=-18.685-2.476*COS(6.28*X/365)+3.574*SIN(6.28*X/365)
0160 LET Y=Y+.674*COS(4*3.14*X/365)+.543*SIN(4*3,14*X/365)
0170 LET Y=Y+.456*COS(6*3.14*X/365)+.893*SIN(6*3.14*X/365)
0180 LET D=INT(Y) 40KM
0190 LET Y=-6 .035-1.498*COS(6.28*X/365)+2.322*SIN(6.28*X/365)
0200 LET Y=Y+1.42*COS(4*3.14*X/365)-.448*SIN(4*3.14*X/365)
0210 LET Y=Y+1.158*COS(6*3.14*X/365)+1.12*SIN(6*3.14*X/365)
0220 LET Y=Y+.499*COS(8*3.14*X/365)+.262*SIN(8*3.14*X/365)
0 240 LET E=INT(Y) 45KM
0250 LET Y=-4.032-1.766*COS(6.28*X/365)+1.402*SIN(6.28*X/365)
0260 LET Y=Y+.516*COS(4*3.14*X/365)-1.691*SIN(4*3.14*X/365)
0270 LET Y=Y+.707*COS(6*3.14*X/365)+.214*SIN(6*3.14*X/365)
0280 LET Y=Y+.317*COS(8*3.14*X/365)~.235*SIN(8*3.14*X/365)
0 290 LET F=INT(Y) 50KM
0300 LET Y=-9.182-1.738*COS(6.28*X/365)+1.007*SIN(6.28*X/365)
0310 LET Y=Y-1.202*COS(4*3.14*X/365)-1.488*SIN(4*3.14*X/365)
0320 LET Y=Y+.241*COS(6*3.14*X/365)-.268*SIN(6*3.14*X/365)
0330 LET Y=Y+.113*COS(8*3.14*X/365)-.907*SIN(8*3.14*X/365)
0 340 LET G=INT(Y) 55KM
```

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0350 LET Y=-16.224+.0917*COS(6.28*X/365)+.781*SIN(6.28*X/365)
0360 LET Y=Y-1.573*COS(4*3.14*X/365)-1.376*SIN(4*3.14*X/365)
0370 LET Y=Y+.0426*COS(6*3.14*X/365)-.139*SIN(6*3.14*X/365)
0380 LET Y=Y-.204*COS(8*3.14*X/365)-.642*SIN(8*3.14*X/365)
0390 LET Y=Y-.719*COS(31.4*X/365)+.338*SIN(31.4*X/365)
0400 LET H=INT(Y) 60KM
0410 LET Y=-24.206+2.932*COS(6.28*X/365)-.0541*SIN(6.28*X/365)
0420 LET Y=Y-1.185*COS(4*3.14*X/365)-.5234*SIN(4*3.14*X/365)
0430 LET Y=Y-.7445*COS(6*3.14*X/365)-1.687*SIN(6*3.14*X/365)
0440 LET Y=Y+.826*COS(8*3.14*X/365)+.386*SIN(8*3.14*X/365)
0450 LET Y=Y-.859*COS(31.4*X/365)-.119*SIN(31.4*X/365)
0 460 LET I=INT(Y) 65KM
0465 IF X>1 THEN GOTO 0490
0470 PRINT " J 25 30 35 40 45 50 55 60 65"
0490 PRINT X; A; B; C; D; E; F; G; H; I
0500 LET X=X+5
0505 IF X>365 THEN GOTO 0520
     GOTO 0010
0510
0520
     STOP
```

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opposite to the Section I data where plus is vest and south distribute

SECTION II PART 2

E-W WIND COMPONENT CHANGEOVER CASES AT WSMR

Changeover of the E-W wind component at WSMR from 25km to 65km is considered for four cases - 1969, 1970, 1972, and 1974. These cases are arbitrarily chosen for convenience and not because of special features. The next step is to establish changeover criteria for more objective timing.

Since the level from 25km to 30km changes only slightly, 30km to 65km will be used for the changeover criteria. The following criteria presented a reasonable approach although some subjectiveness is still present.

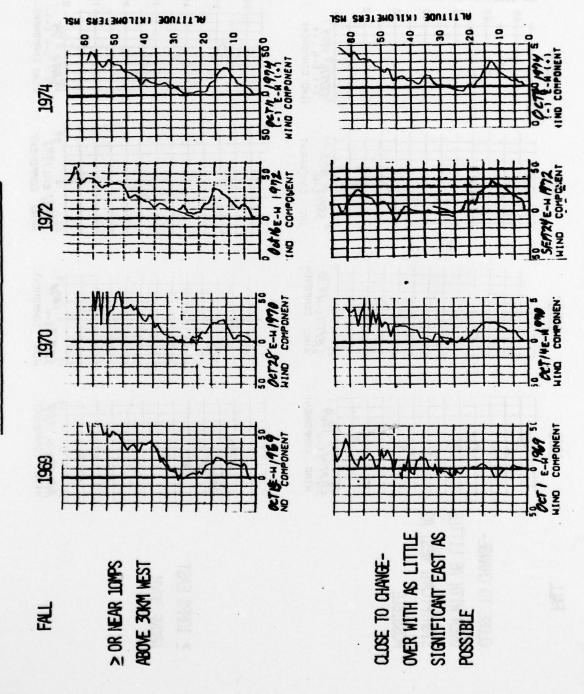
- C >10mps above 30km
- I Close as possible to zero without significant changeover
- T
- E Close as possible to zero after changeover
- D
- ≥10mps above 30km after changeover

The greatest change occurs in the 50-65km region and decreases to 25km. Averages of the four cases give a fall changeover from September 10 to October 4 with a 24 day transition (Figure 26). The spring changeover average is April 16 to May 11 or 25 days (Figure 27).

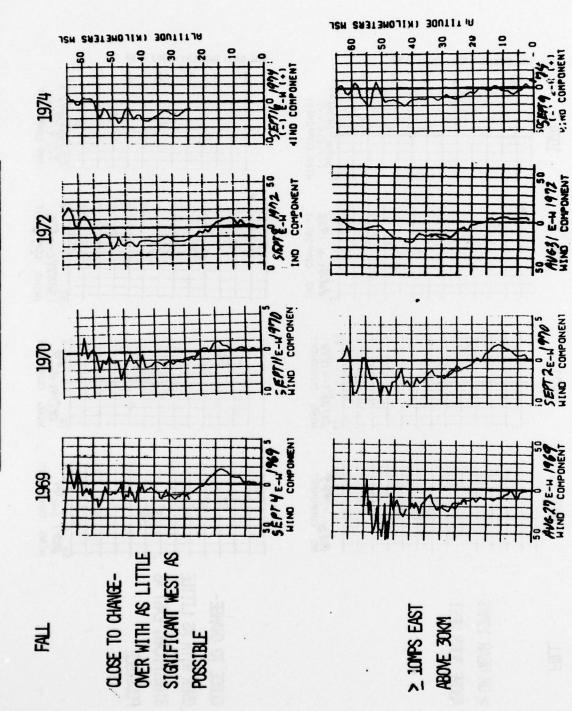
Our model of the changeover (Table 13) shows a fall changeover from September 14 to October 8 or 24 days and a spring changeover from April 20 to May 5 or 15 days. The shorter spring changeover is not confirmed by the four cases. Because of the many subjective factors, no conclusion can be drawn about the relative length of spring and winter changeover periods.

NOTE: The negative sign following a number means west wind in meters per second and a positive number is east wind (mps) - this convention is opposite to the Section I data where plus is west and south directions.

The Data Section follows the convention of reference 12.



WIND COMPONENT IN METERS/SEC.

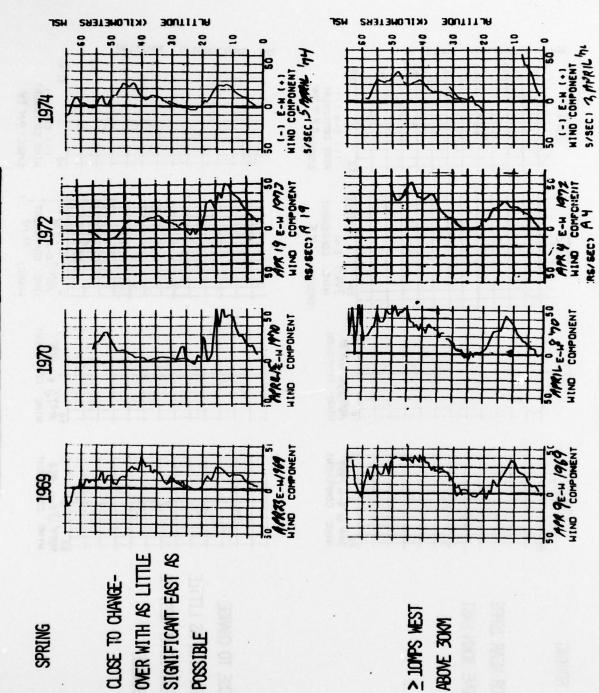


WIND COMPONENT IN METERS/SEC.

WIND COMPONENT IN METERS/SEC.

SYSECT 9M 94

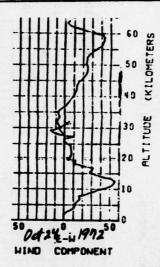
SYSECO MITTI



WIND COMPONENT IN METERS/SEC.

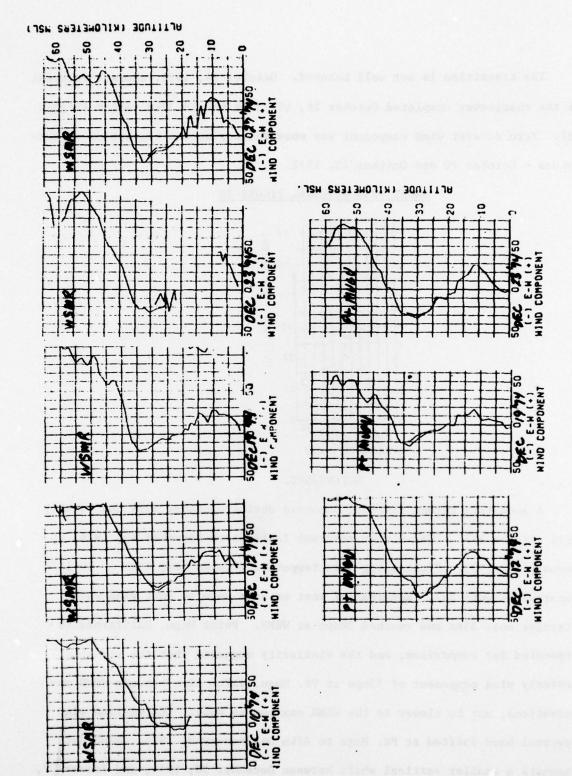
The transition is not well behaved. October 24, 1972, shows a reversal of the changeover completed October 16, 1972, in the 28-37km region (Figure 28). Zero or west wind component was observed during two bracketing rocket-sondes - October 20 and October 25, 1972.

SHORT TERM REVERSAL FIGURE 28



METERS/SEC.

A long term strong reversal occurred during December 1974 and January 1975 (Figure 29). This winter reversal lasted from December 10, 1974, to January 14, 1975. Fluctuating warm temperature peaks near 46km of 10-15°C occurred (Figure 30). Reversal of west or near zero to east wind was stronger near 35km and reached 30mps at WSMR. Point Mugu, California is presented for comparison; and the similarity suggests that the strongest easterly wind component of 55mps at Pt. Mugu, which lies between WSMR observations, may be closer to the WSMR maximum as well. The maximum wind reversal band shifted at Pt. Mugu to 47km on January 3, 1975. WSMR data suggests a smaller vertical shift between December 30, 1974, and January 7, 1975.

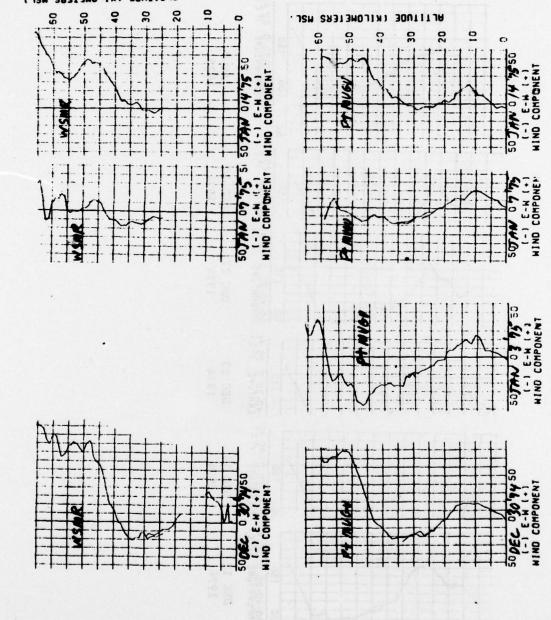


ALTITUDE INT. ONETERS MSL1

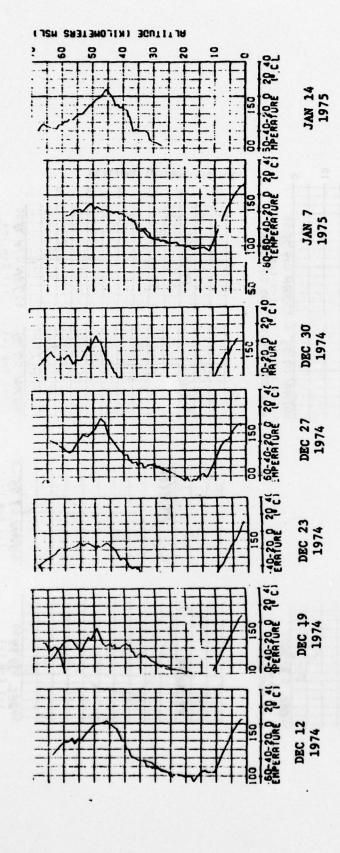
9

+ 20

+ 30



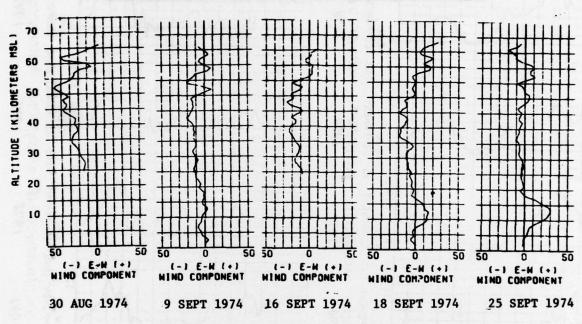
TEMPERATURE PROFILE AT WINE DURING LONG TERM REVERSAL FIGURE 30

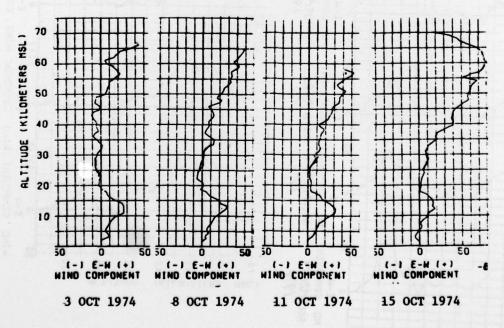


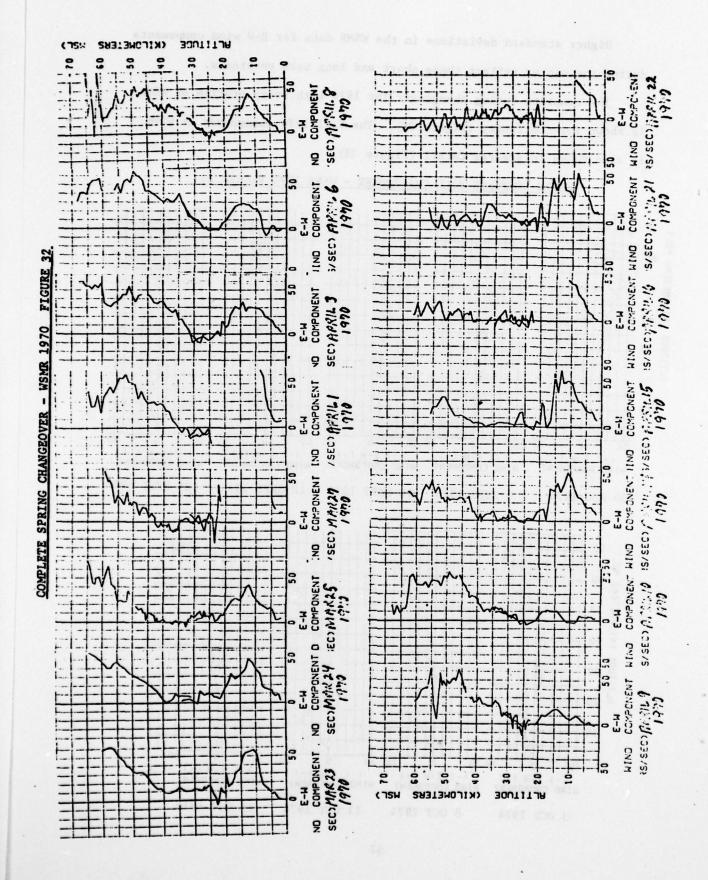
Higher standard deviations in the WSMR data for E-W wind components during the winter reflect these short and long term reversals.

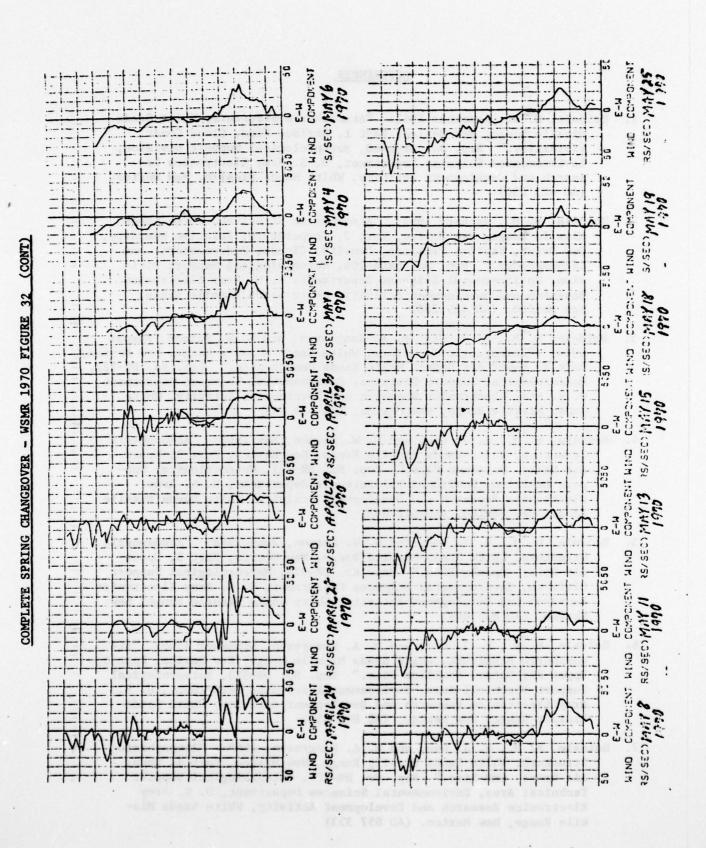
The complete spring changeover for 1970 with every profile at WSMR is shown for continuity (Figure 32). The fall 1974 changeover at WSMR is also shown in greater detail (Figure 31).

NEARLY COMPLETE FALL CHANGEOVER - WSMR 1974 FIGURE 31









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